

TOTAL ENERGY SYSTEM FOR WATER REUSE
AND CONCENTRATION OF MIXED WASTE WATERS

for

E G & G ROCKY FLATS
P.O. 83115M
SEPTEMBER 20, 1990

Prepared by

W.R. WILLIAMSON
CHIEF OF RESEARCH & DEVELOPMENT

for

LICON JOB ORDER 901

LICON, INC.
P.O. BOX 10717
PENSACOLA, FLORIDA 32524

OCTOBER 15, 1990

ADMIN RECORD

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EXECUTIVE SUMMARY

Mixed hazardous wastes with low level radioactivity presently stored at weapon sites in ponds and drums etc. can employ technologies funded by the Department of Energy, Office of Industrial Programs under contract DE-AC07-79CS40290 to dewater, reuse and concentrate industrial waste water in an energy effective way. Copies of the final report DE-86007851 are available from DOE Technical Information Center, Oak Ridge, TN. One of the heat pump designs developed under this contract is depicted in Figure 1. LICON has since expanded this effort with the application of the MEMS (Multiple Effect Multi Stage) distillation system, Figure 2, to further concentrate the waste and attain the mandate for waste minimization.

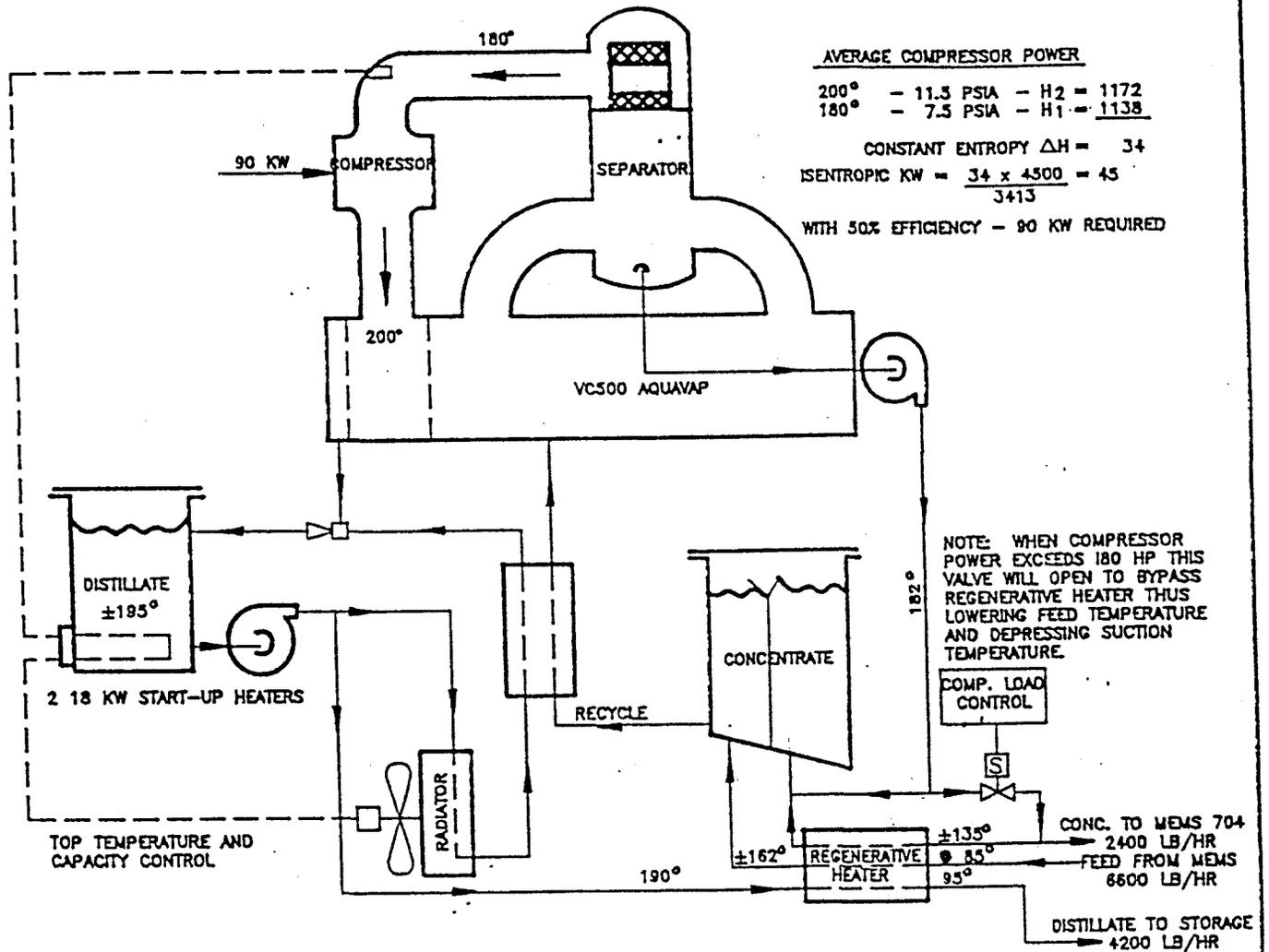
The recent energy crisis has added impetus to also minimize energy consumption. A total energy system depicted in Figure 3 can employ domestic natural gas to fuel internal combustion engines and furnish electric power to Figure 1. The heat that is normally wasted in power generation to the engine jackets and exhaust can be employed to operate the MEMS cycle depicted in Figure 2. All of the components of the total energy system are in active use with proven track records. Their combination can reduce both energy and capital cost of heretofore custom designed distillation plants by at least 50%.

In modular design, these LICON's (LIquid CONcentrators) not only save energy, their self sufficiency allows for trailer mounting for emergency deployment. They can furnish power to, and concentrate blow-down from, membrane processes such as reverse osmosis and electro dialysis or from ion exchange. Their production

of high purity distillate, less than 75 ppm for reuse and their ability to concentrate liquid waste in excess of 500,000 ppm and in many cases recover precipitated salts provides an economical method of waste minimization. Further use can be made of the waste heat to dry the concentrated sludge to a powder.

The attached report covers the investigation of simulated Rocky Flats pond waters and established criteria to substantiate the quality of distillate and degree of concentration cited above. Evaluation of the test results would indicate that 10,000 ppm feed (pond average) could be reduced to 1/50th of the present volume and produce an excellent quality of distillate averaging less than 75 microsiemens and under more steady state conditions there were indications of being able to achieve less than 20 microsiemens with alkalinity control. Run off water averaging less than 5,000 ppm could be reduced by 1/100th. No data was taken to evaluate the effect of radioactivity.

TRANSVAP 750 - AQUAVAP VC500 HEAT BALANCE



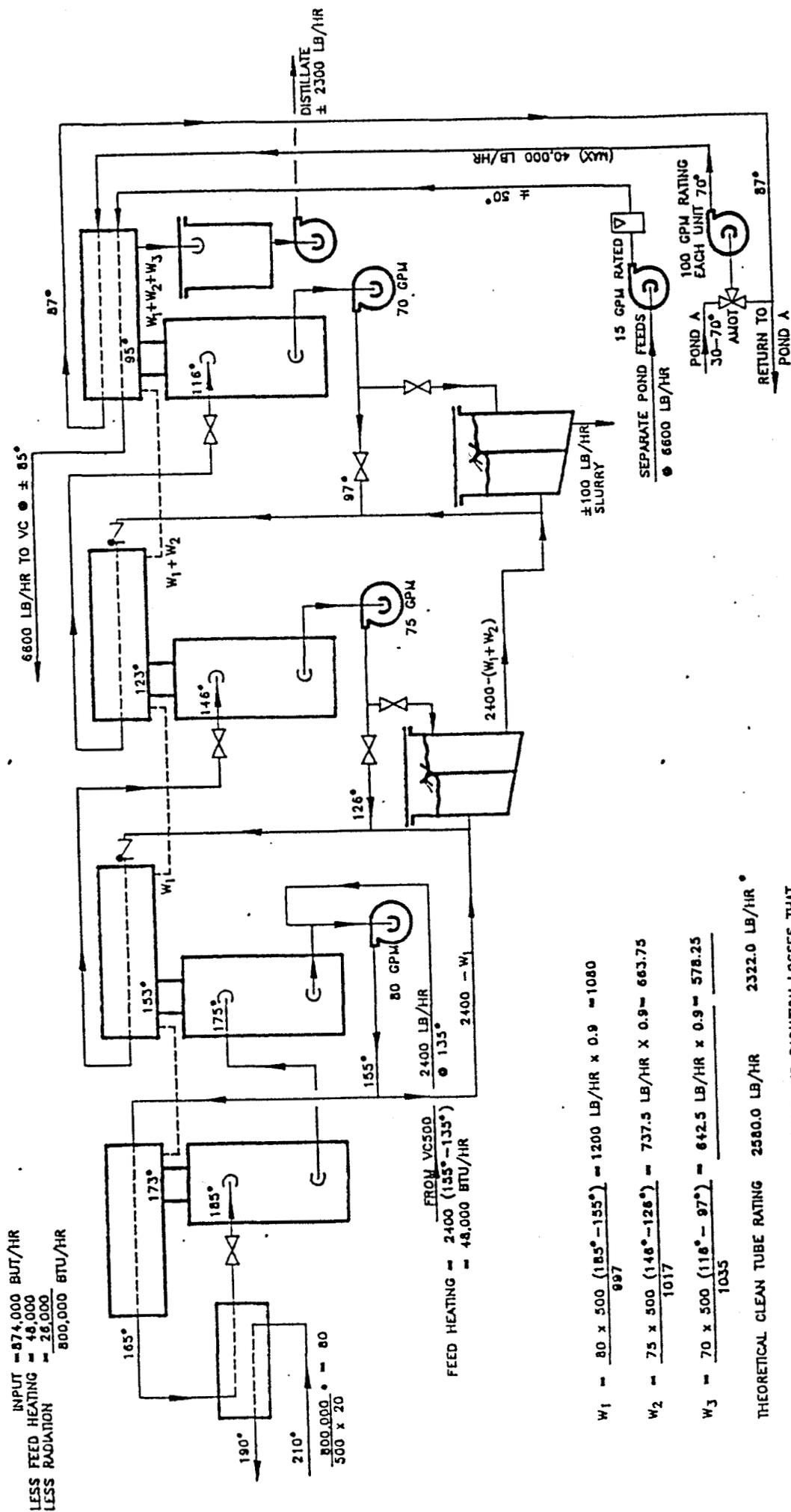
HEAT TRANSFER RATE REVIRED WITH 2° BOILING POINT ELEVATION AND SEPARATION LOSSES + 300 LB/HR DESUPERHEAT WATER

$$U_R = \frac{4,500,000}{18 (\Delta T) \times 470 \text{ SQ.FT.}} = 530 \text{ BTU/HR/SQ.FT./}^\circ\text{F}$$

$$\text{FEED HEATING REQUIRED} = 6600(182-182) = 132,000 \text{ BTU/HR} = 38.88 \text{ KW}$$

DISCOUNTING RADIATION AND VENT LOSSES, RADIATOR WILL HAVE TO DISSIPATE MAXIMUM OF 50 KW

HEAT BALANCE FOR AVERAGE CONDITIONS - TRANSVAP 750 MEMS 704 RATED 250 GPH



INPUT = 874,000 BTU/HR
 LESS FEED HEATING = 48,000
 LESS RADIATION = 26,000
 800,000 BTU/HR

FROM VC500
 FEED HEATING = 2400 (155° - 135°)
 = 48,000 BTU/HR

$$\begin{aligned}
 W_1 &= \frac{80 \times 500 (185^\circ - 155^\circ)}{997} = 1200 \text{ LB/HR} \times 0.9 = 1080 \\
 W_2 &= \frac{75 \times 500 (146^\circ - 126^\circ)}{1017} = 737.5 \text{ LB/HR} \times 0.9 = 663.75 \\
 W_3 &= \frac{70 \times 500 (116^\circ - 97^\circ)}{1035} = 642.5 \text{ LB/HR} \times 0.9 = 578.25
 \end{aligned}$$

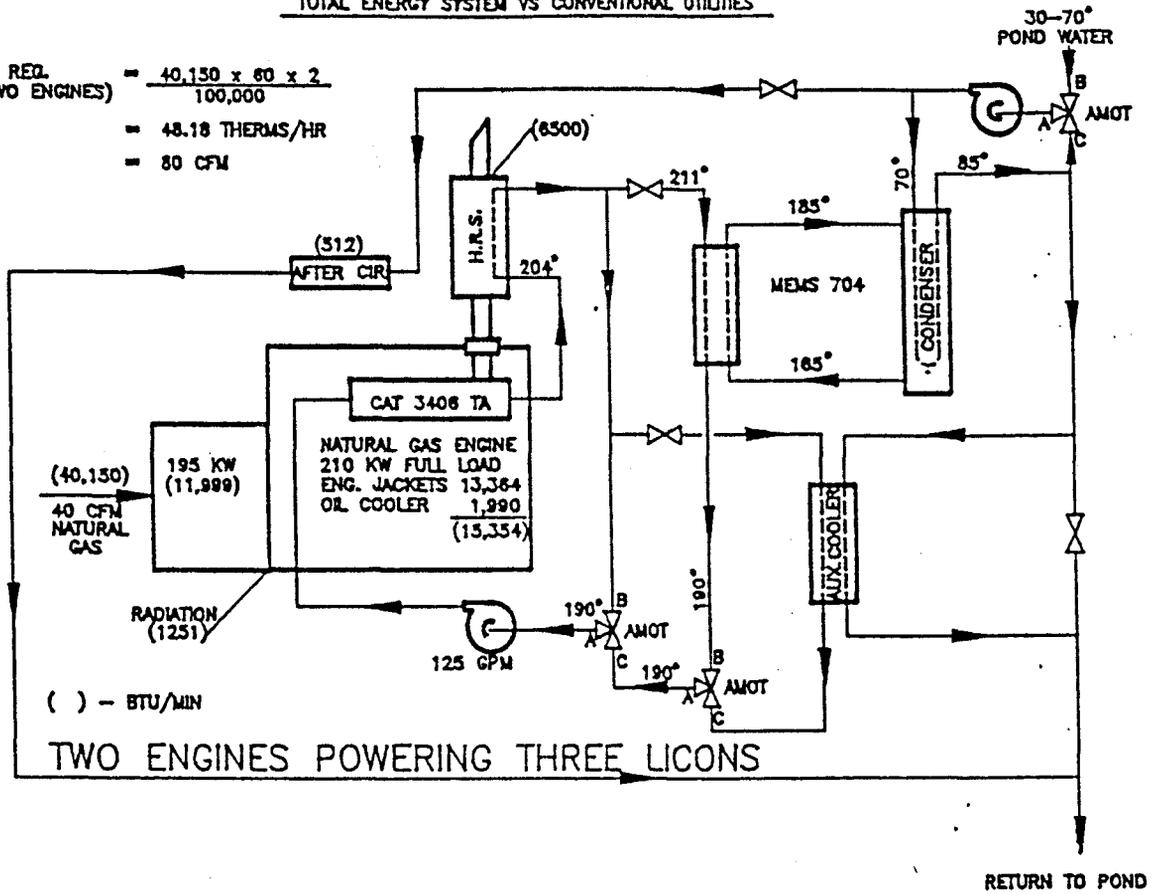
THEORETICAL CLEAN TUBE RATING 2580.0 LB/HR 2322.0 LB/HR*

* FROM EXPERIENCE, THERE WILL BE VENT AND RADIATION LOSSES THAT WILL REDUCE CAPACITY BY APPROXIMATELY 10%.

TRANSVAP 750 HEAT BALANCE PROPOSED FOR ROCKY FLATS

TOTAL ENERGY SYSTEM VS CONVENTIONAL UTILITIES

- ① ENERGY REQ. (FOR TWO ENGINES) = $\frac{40,150 \times 60 \times 2}{100,000}$
 = 48.18 THERMS/HR
 = 80 CFM



TWO ENGINES POWERING THREE LICONS

| RECOVERABLE | NON RECOVERABLE | LOSSES | AVERAGE POWER REQUIRED |
|-------------------------------|-----------------|---------------|------------------------|
| JACKETS - 13,364 | POWER 11,999 | 40,150 INPUT | VC-500 - 90 KW (COMP) |
| OIL COOLER - 1,990 | RADIATION 1,251 | - 21,854 | MEMS - 20 |
| EXHAUST - 6,500 | AFTER CIR. 512 | - 13,762 | AUXILIARIES - 20 |
| 21,854 BTU/MIN | 13,762 BTU/MIN | 4,534 BTU/MIN | 130 x 3 |
| x 60 x 2 | | | = 390 KW |
| 3 2,622,480 BTU/HR RECOVERY | | | |
| = 874,160 BTU/HR TO EACH MEMS | | | |

EQUIVALENT COST OF STEAM WITH 85% BOILER EFFICIENCY = $\frac{2,622,480}{0.85 \times 100,000}$ = 30.85 THERMS/HR

EQUIVALENT COST OF ELECTRIC POWER = 390 KW x \$.08 = \$31.20

$\frac{53.25 \text{ THERMS/HR}}{84.10 \text{ THERMS/HR}} = ①$

- GAS COST @ 30.85 x \$.85/THERM = \$20.00
 - ENGINE FUEL = 48.18 x \$.85 = \$31.32
 - (EQUIVALENT TO DIESEL OIL @ \$1.00/GALLON)
 - (AT 25% STATION & TRANSMISSION EFFICIENCY)
- \$51.20
\$19.88/HR SAVINGS

INCREMENTAL COST OF ENGINES = $\frac{\$85,000}{19.88}$ = 3772 HRS = 25 1/2 WEEKS PAY BACK

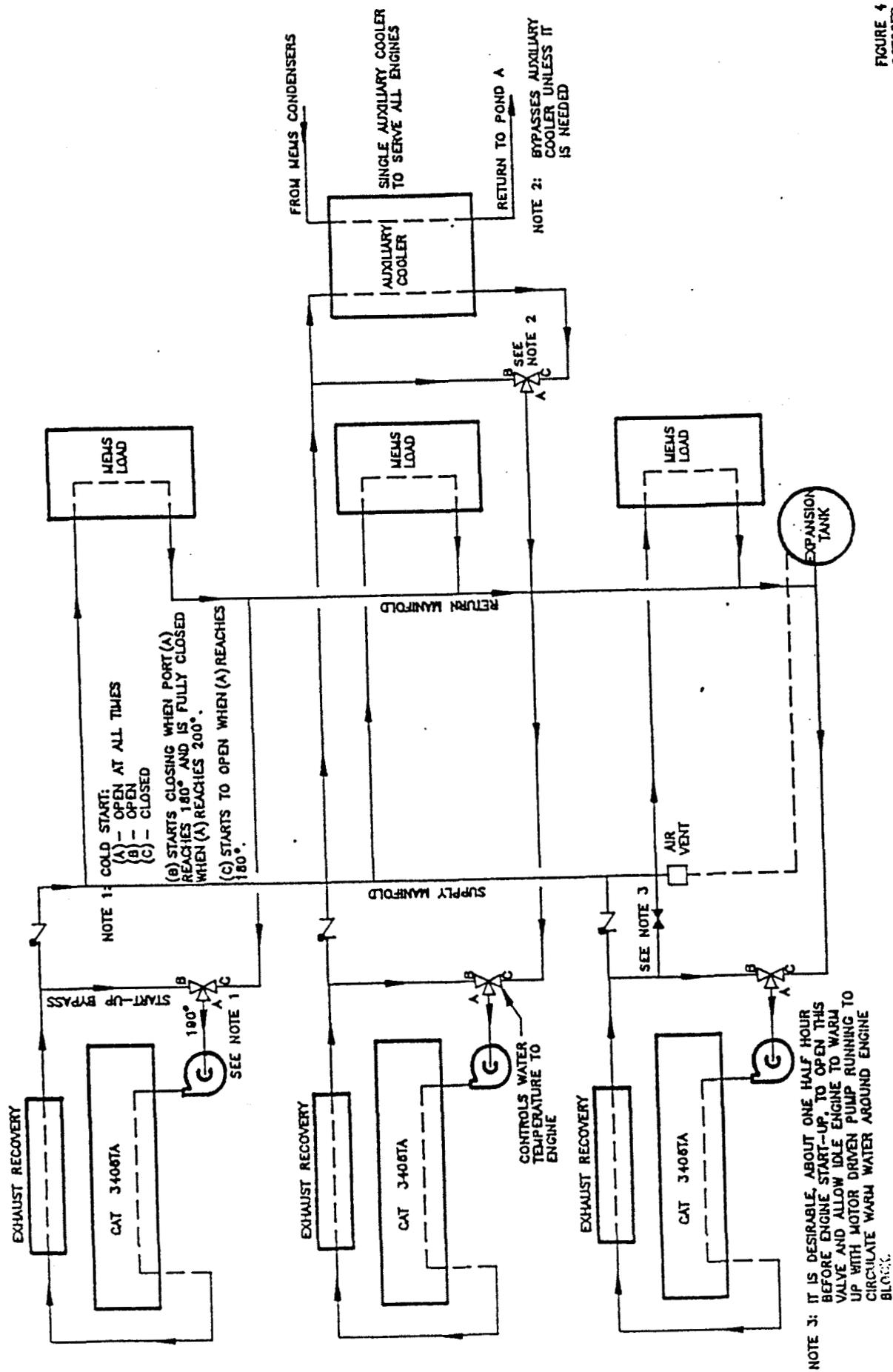
NOTE 1 - THIS TOTAL ENERGY CONCEPT PROJECTS CUTTING ENERGY CONSUMPTION IN ALMOST HALF AND USES DOMESTIC NATURAL GAS

NOTE 2 A CONVENTIONAL FOUR EFFECT STEAM OPERATED PLANT WITH A PERFORMANCE RATIO OF 3 TO 1 WOULD CONSUME $\frac{3 \times 750 \times 8.33 \times 1000}{3 \times 100,000 \times 0.8 \text{ (BOILER EFF)}}$ = 78.00 THERMS/HR

PLUS AUXILIARY ELECTRIC POWER OF 100 KW EQUIVALENT TO $\frac{13.65 \text{ THERMS/HR}}{91.65 \text{ THERMS/HR}}$

ENGINE COOLING WATER ARRANGEMENT

FOR TWO ENGINES RUNNING AND ONE STANDBY



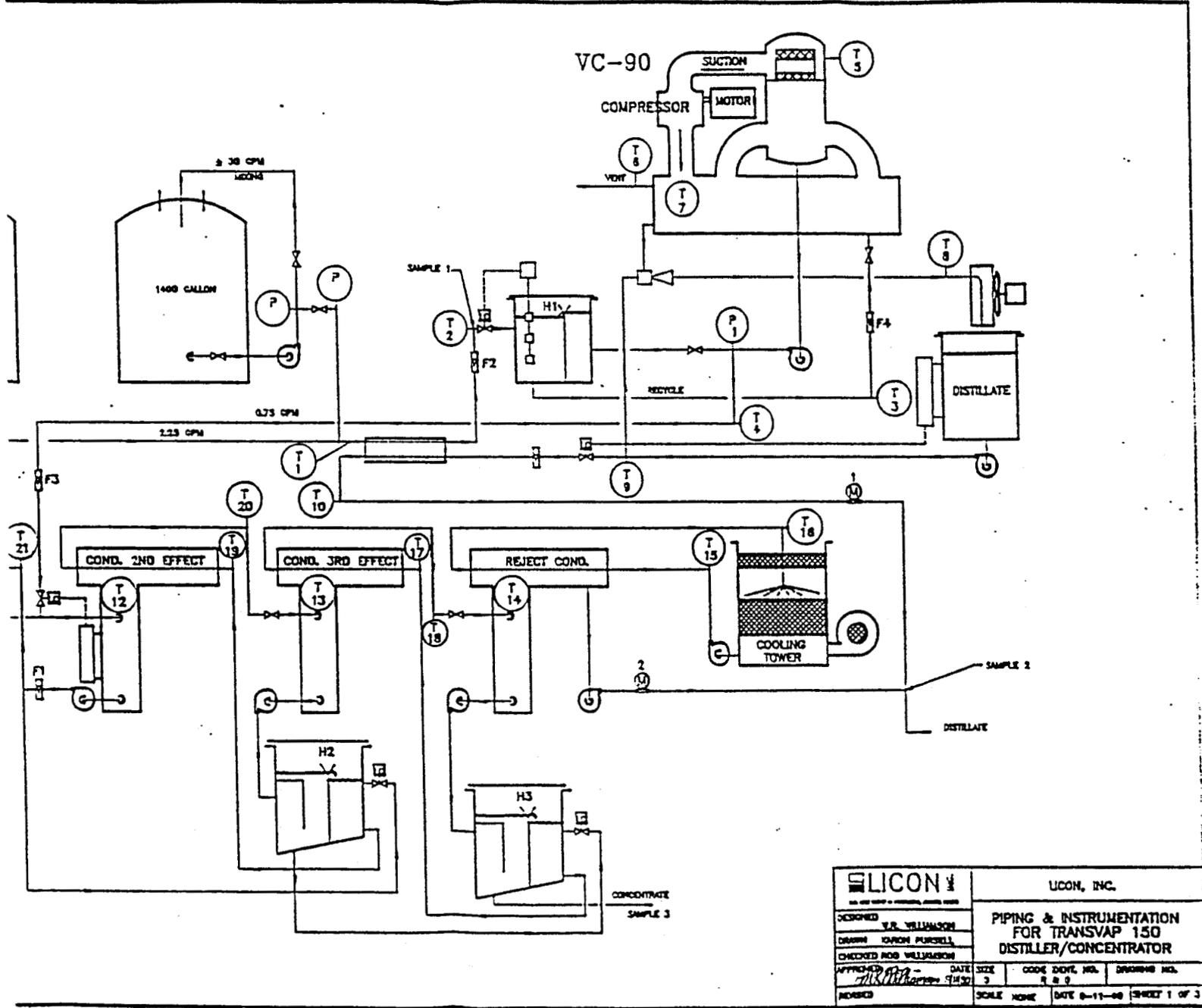
TEST SUMMARY USING SIMULATED ROCKY FLATS POND WATER

E G & G prepared a test agenda outline in the Appendix 'A' as 'LICON EVAPORATOR TEST REQUIREMENTS'. Anticipating problems in achieving the degree of concentration required, LICON prepared a supplement Appendix 'B' including a P & I diagram dated 10 September 1990 (Fig. No. 5).

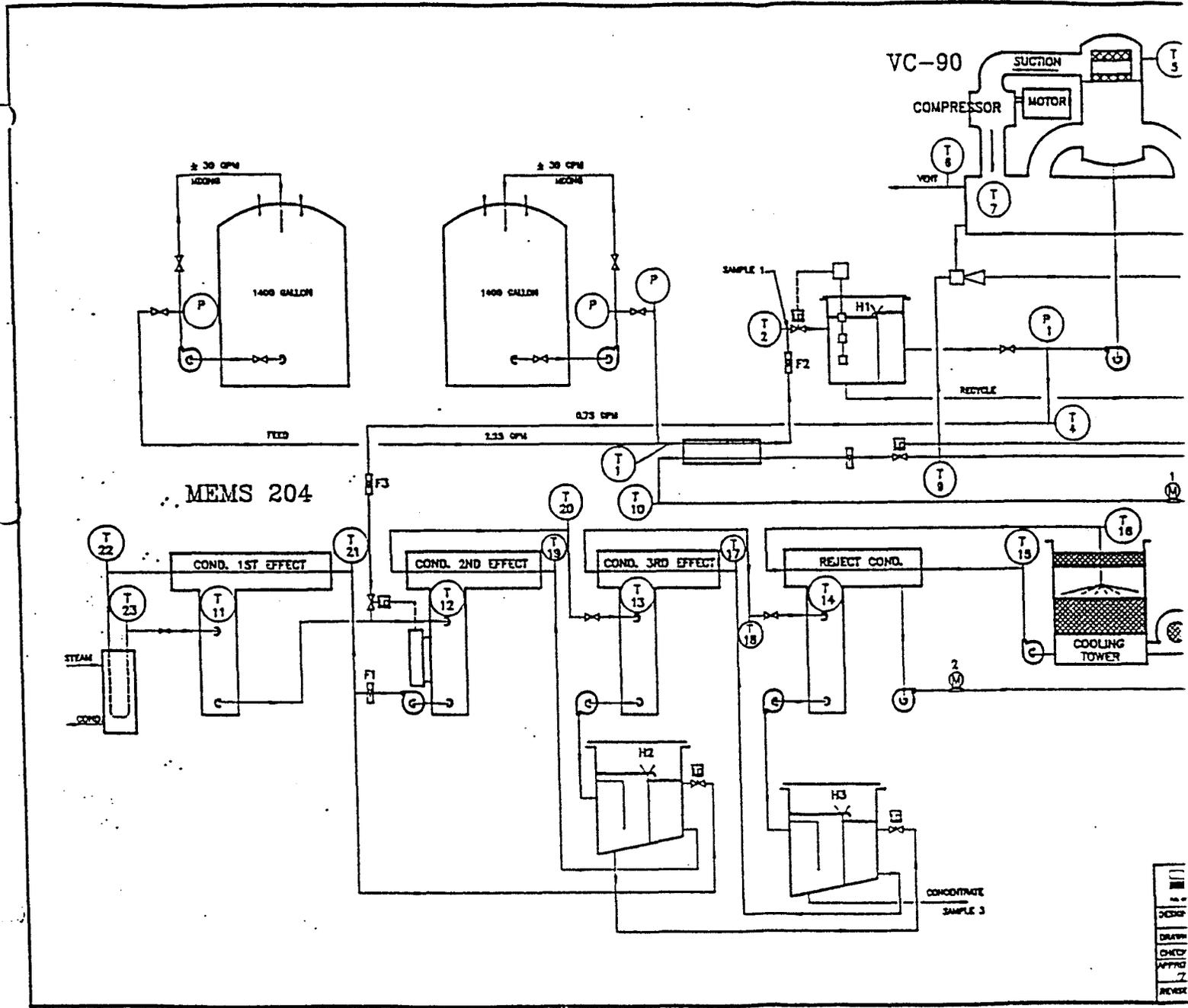
Test No. 1, September 13 1990

Pond A water was tested in accordance with above as detailed in the report in the Appendix 'C'. In essence, this test revealed how complex these pre-trial tests were going to be if we wanted to attain some indication of the concentration ratios to be expected in the field. The chloride readings made us suspicious of the chemical analysis done by the local testing laboratory, Analytic Technologies (1), so we had Rob Farrell of ChemTreat do some testing with his HACH KIT (2). See Table No. 1

Except for the Chloride differences in the Feed and the Concentrate there was some good correlation in the distillate analysis. If Analytic's TDS is correct and Farrell's conductivity is correct then the factor to convert from MS to TDS is 0.825 which in turn does not seem to apply to the distillate which is 2.93. In any event the distillate is good but the concentration ratio is low, and will require further modification of the test procedure. The chemical results are averages for the entire run in accordance with E G & G test requirements. The final concentration was actually closer to 10 to 1 - still not good enough. Listed in the attached detailed report Appendix 'C' are the modifications we made to attain higher concentration ratios including sampling pots to more closely track the distillate quality.



| | | | |
|----------------|--------------------|--|---------|
| SILICON | | LICON, INC. | |
| DESIGNED | V.R. WILLIAMSON | PIPING & INSTRUMENTATION FOR TRANSVAP 150 DISTILLER/CONCENTRATOR | |
| DRAWN | EDMON PURCELL | DATE | 9 13 50 |
| CHECKED | ROB WILLIAMSON | SIZE | 9 2 |
| APPROVED | <i>[Signature]</i> | CODE DEPT. NO. | 9 2 |
| NOTED | | SCALE | NONE |
| | | DATE | 8-11-50 |
| | | SHEET | 1 OF 3 |



DRAWN
 CHECKED
 APPROVED
 REVER

Revision 1

TEST NO. 1, JOB 901 - ROCKY FLATS SYNTHETIC POND A WATERSummary of Test Results and Conclusions

Initial test required the following list of chemicals mixed in a 1400 gallon tank full of Pensacola city water during the evening of 12 September 1990, under the direction of engineers from Rocky Flats.

| | <u>lb/1000 Gal.</u> | <u>lb/1400 Gal.</u> | <u>Grams added</u> |
|---|---------------------|---------------------|--------------------|
| Calcium Nitrate [Ca(NO ₃) ₂ 3 H ₂ O] | 2.5 | 3.5 | 1587.6 |
| Sodium bicarbonate (Na H CO ₃) | 0.42 | 0.6 | 272 |
| Potassium Chloride (KCI) | 4.1 | 5.75 | 2608 |
| Sodium Carbonate (Na ₂ CO ₃ H ₂ O) | 0.1 | 0.14 | 63.5 |
| Sodium Nitrate (Na NO ₃) | 4.2 | 5.9 | 2676 |
| Magnesium Sulfate (Mg SO ₄ 7 H ₂ O) | 6.75 | 9.5 | 4309 |
| Sodium Hydroxide (Na OH) | | | 500 |

pH = 9.3

This initial test was started at 0700 on 13 September 1990. Both the VC 90 and the MEMS 204 were filled to operating levels requiring 400 gallons of the above solution. Start-up was somewhat erratic because the maximum amount of feed attainable was only 3 GPM even with the feed solenoids bypassed. When the VC came on line it was making in excess of 100 GPH and there was not enough blowdown to satisfy the demand of the MEMS unit which was also having problems with interrupted steam supply due to a faulty fire-eye. The VC 90 capacity was cut back slightly by lower the suction temperature adjustment to the compressor; also the MEMS top temperature was reduced and thus combined capacity was lowered from 200 GPH to the target capacity of 150 GPH (1/5th Rocky Flats size).

MBB 18 Sep 1990

The operators got used to compensating for the low feed rates and the run was successfully completed. By shutting down the VC and using its residue to feed the MEMS and then shutting down the MEMS when it reached critical low levels for adequate circulation, the residue was reduced from 400 gallons to less than 200. We then made some piping changes and rigged to pump out the top two stages to the third stage. The top two stages were rigged to operate on city water at 1400 hr. This procedure enabled us to dewater the 1400 gallons down to 104 gallons. Samples of the final residue were collected for chemical analysis. This initial test indicated the desirability of making the following changes to achieve greater concentration ratios and to acquire better distillate quality.

1. Since we were only able to acquire about 14 to 1 concentration ratio, the Rocky Flats engineers provided the following higher weight listing of chemicals for our next test.

| | <u>lb/1000 gal.</u> | <u>lb/1400 gal.</u> |
|--------------------|---------------------|---------------------|
| Calcium Nitrate | 2.5 | 3.5 |
| Sodium bicarbonate | 5.0 | 7.0 |
| Potassium Chloride | 20.0 | 28.0 |
| Sodium Carbonate | 7.5 | 10.5 |
| Sodium Nitrate | 38.0 | 53.2 |
| Magnesium Sulfate | 30.0 | 42.0 |

pH = 7.5

2. The VC distillate was not as good as the MEMS distillate so we decided to try a single, denser mesh to replace our standard two stage lower density mesh. This change had been effective at Blue Bird Body where there are 2-VC 600's in operation on alkaline waste water.
3. Sampling pots similar to those used on the test of the VC 300 for Three Mile Island were added to the eductor suction of the VC 90 and to the fourth stage eductor suction of the MEMS 204. These were added to assure that there was no downstream contamination from regenerative heaters or pump seals. Any leakage at these sources however would be in the other direction since the distillate pressure is normally higher than the concentrate. Because of step 4 however we thought this would be a good idea and sampling under vacuum might provide a clue as to any gaseous carry-over.
4. A higher pressure feed pump was added to alleviate the problems associated with low feed rates.

JRZ 18 Sept 30

5. The start-up procedure was changed. Only the VC 90 would be filled from the feed tank and then run at full capacity blowing as much of its resultant concentrate to the MEMS until the MEMS was full of VC concentrate. Only then would the MEMS be started and thus would be operating on higher density feed stock. This also would allow easier start-up since the MEMS would not be robbing heat from the VC while steady state conditions were being achieved.

cc: L. Eng - Rocky Flats
C. Hughes - Licon
R. Williamson - Licon

NOTE: This revision 1 corrects errors on page 2 of FAX
sent to Mr. Eng 9.17.90

ARR 19 Sept 90

LOG SHEET ON ROCKY FLATS POND WATER TESTS

JOB NO. 901

POND WATER A

DATE: 9-13-90

| TIME: | 7:00 | 7:30 | 8:00 | 8:30 | 9:00 | 9:30 | 10:00 | 10:30 | 11:00 |
|-------------------------|----------|----------|----------|----------|-----------|-----------|-----------|-----------|-----------|
| TEMPERATURES: | | | | | | | | | |
| T1 FEED SUPPLY | 84 | 84 | 84 | 84 | 84 | 84 | 84 | 84 | 84 |
| T2 FEED TO VC | 134 | 201 | 130 | 130 | 127 | 136 | 119 | 140 | 141 |
| T3 VC RECYCLE FEED | 172 | 187 | 166 | 172 | 178 | 170 | 174 | 172 | 176 |
| T4 BLOWDOWN TO MEMS | 123 | 160 | 168 | 164 | 165 | 166 | 161 | 166 | 166 |
| T5 VC SUCTION | 148 | 176 | 172 | 170 | 175 | 174 | 171 | 170 | 171 |
| T6 VC VENT | 158 | 193 | 182 | 185 | 190 | 190 | 188 | 186 | 188 |
| T7 VC CHEST | 155 | 195 | 185 | 187 | 192 | 191 | 189 | 188 | 190 |
| T8 VC EDUCTOR DISCH. | 146 | 186 | 174 | 182 | 188 | 188 | 186 | 186 | 185 |
| T9 VC DISTILLATE IN HX | 142 | 175 | 165 | 179 | 182 | 182 | 180 | 181 | 180 |
| T10 VC DIST. OUT HX | 100 | 92 | 99 | 96 | 99 | 100 | 94 | 98 | 98 |
| T11 1ST FLASH VAPOR | 155 | 160 | 156 | 149 | 155 | 154 | 161 | 169 | 168 |
| T12 2ND FLASH VAPOR | 148 | 157 | 152 | 143 | 150 | 149 | 152 | 157 | 159 |
| T13 3RD FLASH VAPOR | 129 | 130 | 132 | 134 | 132 | 130 | 132 | 133 | 133 |
| T14 4TH FLASH VAPOR | 78 | 111 | 134 | 136 | 134 | 129 | 126 | 118 | 116 |
| T15 COOLANT INLET | 77 | 99 | 88 | 88 | 88 | 84 | 84 | 100 | 101 |
| T16 COOLANT OUTLET | 74 | 108 | 88 | 88 | 88 | 94 | 100 | 108 | 110 |
| T17 4TH FLASH CONC. | 90 | 111 | 123 | 121 | 130 | 120 | 124 | 116 | 116 |
| T18 4TH FLASH FEED | 101 | 127 | 132 | 133 | 133 | 128 | 131 | 128 | 129 |
| T19 3RD FLASH CONC. | 132 | 138 | 140 | 141 | 145 | 140 | 140 | 140 | 141 |
| T20 3RD FLASH FEED | 146 | 154 | 147 | 144 | 145 | 145 | 149 | 151 | 152 |
| T21 2ND FLASH CONC. | 147 | 156 | 150 | 142 | 143 | 145 | 154 | 156 | 156 |
| T22 FEED TO HTR. | 155 | 160 | 156 | 151 | 159 | 152 | 159 | 161 | 161 |
| T23 OUTPUT FROM HTR. | 161 | 178 | 167 | 155 | 155 | 161 | 165 | 168 | 170 |
| F1 FIRST STAGE RECYCLE | 40GPM | 40GPM | 15 | 22GPM | 40 | 25GPM | 40GPM | 40 | 40GPM |
| F2 VC FEED RATE | 1.0 | 3/4 | 3/4 | 3/4 | 1.3 | 3/4 | 1 3/4 | 3/4 | 3/4 |
| F3 VC BLOWDOWN | .8 | 1.0 | .4 | 1.0 | 0 | 1.3 | 1.0 | 1.0 | 1.2 |
| F4 VC RECYCLE | 2 3/4 | 3 3/4 | 3.5 | 3.5 | 3.5 | 3 3/4 | 4 | 3.5 | 3.5 |
| H1 VC BRINE WEIR | 1" | 1" | 1" | 1" | 3/4" | 1" | 1" | 1" | 1" & 2" |
| H2 3RD STAGE WEIR | 2 1/4 | 2 1/4 | 2 1/4 | 2 1/4 | 2 3/4 | 3" | 3" | 3" | 3 1/4 |
| H3 4TH STAGE WEIR | 2 1/4 | 2 1/4 | 2 1/4 | 2 1/4 | 2 3/4 | 3" | 3" | 3" | 3 1/4 |
| FEED TANK LEVEL | | 1000 | 825 | 825 | 725 | 675 | 625 | 550 | 450 |
| M1 VC DISTILLATE 459 | (1) 442 | (3) 505 | (2) 562 | (1) 602 | (4) 645 | (5) 702 | (4) 749 | (2) 777 | (6) 736 |
| M2 MEMS DISTILLATE 1597 | (2) 1579 | (3) 1581 | (4) 1537 | (1) 1581 | (2) 15924 | (2) 15945 | (3) 15979 | (3) 16015 | (5) 15065 |
| M3 COMBINED DIST. | 11 | 74 | 100 | 54 | 77 | 75 | 81 | 64 | 109 |
| V VOLTAGE | 475 | 475 | 475 | 475 | 475 | 475 | 475 | 475 | 475 |
| A AMPS | 403 | 37 | 34 | 55 | 53.4 | 53.4 | 55.9 | 55.6 | 35 |
| KW KILOWATTS | 32 | 21.3 | 19.5 | 30 | 36.2 | 36.2 | 37 | | |

| DATE: | 9/13/90 | | | | | | | | | |
|----------------------|---------|------|------|------|------|------|------|-------|-------|-------|
| TIME: | 7:00 | 7:00 | 7:30 | 8:00 | 8:30 | 9:00 | 9:30 | 10:00 | 10:30 | 11:00 |
| POND A | | | | | | | | | | |
| CONDUCTIVITY FEED #1 | | | | | | | | ATSC | | |
| DIST. #2 | 48 | 40 | 63 | 64 | 53 | 61 | 56 | 64 | 76.1 | 64 |
| CONC. #3 | | | | | | | | | | |
| pH FEED #1 | 9.3 | 9.2 | 9.3 | 9.4 | 8.9 | 8.9 | 9.1 | 9.1 | 9.0 | 9.0 |
| DIST. #2 | | | | 8.1 | 8.1 | 8.2 | 7.7 | 7.9 | 8.2 | 8.3 |
| CONC. #3 | 9.3 | 9.2 | 9.1 | 9.0 | 8.5 | 8.2 | 8.6 | 8.7 | 8.7 | 8.7 |
| POND BN | | | | | | | | | | |
| CONDUCTIVITY FEED | | | | | | | | | | |
| DIST. | | | | | | | | | | |
| CONC. | | | | | | | | | | |
| pH FEED | | | | | | | | | | |
| DIST. | | | | | | | | | | |
| CONC. | | | | | | | | | | |
| POND BC | | | | | | | | | | |
| CONDUCTIVITY FEED | | | | | | | | | | |
| DIST. | | | | | | | | | | |
| CONC. | | | | | | | | | | |
| pH FEED | | | | | | | | | | |
| DIST. | | | | | | | | | | |
| CONC. | | | | | | | | | | |
| POND BS | | | | | | | | | | |
| CONDUCTIVITY FEED | | | | | | | | | | |
| DIST. | | | | | | | | | | |
| CONC. | | | | | | | | | | |
| pH FEED | | | | | | | | | | |
| DIST. | | | | | | | | | | |
| CONC. | | | | | | | | | | |

Started bring in food to tanks at 5:30. Tank filled by 6:15 started pulling vacuum. Started Compressor v.c. at 6:37. Started steam to flash at 6:40. Tank approx: 300 GAL TO ALL TANKS

LOG SHEET FOR WATER SAMPLES

JOB ORDER

| DATE: | -1/13/90 | | | | | | | | | | |
|-------------------------------|----------|-------|-------|-------|-------|------|-------|-------|-------|-------|------|
| TIME: | 11:30 | 12:00 | 12:30 | 1:00 | 1:30 | 2:00 | 2:30 | 3:00 | 3:30 | 4:00 | 4:30 |
| POND A. | | | | | | | | | | | |
| 1A MK CONDUCTIVITY FEED #1 | 2.56 | 2.67 | 2.67 | 2.57 | 2.57 | - | - | - | - | - | - |
| Combined DIST. #2 | 50.0 | 52.5 | 51.5 | 46.2 | 51.3 | 21.8 | - | - | - | - | - |
| ms/cm CONC. #3 | 6.73 | 8.00 | 9.45 | 10.65 | 11.87 | 9.97 | 13.83 | 14.41 | 16.19 | 19.14 | - |
| pH FEED #1 | 8.9 | 8.9 | 8.9 | 8.8 | 8.8 | - | - | - | - | - | - |
| Combined DIST. #2 | 8.1 | 8.1 | 7.8 | 7.5 | 7.5 | 8.2 | 8.2 | 7.8 | 7.5 | 7.5 | 7.5 |
| 7/MSH CONC. #3 | 8.7 | 8.7 | 8.7 | 8.7 | 8.7 | 8.7 | 8.6 | 8.2 | 8.5 | 8.6 | 8 |
| POND BN | | | | | | | | | | | |
| CONDUCTIVITY FEED | | | | | | | | | | | |
| DIST. | | | | | | | | | | | |
| CONC. | | | | | | | | | | | |
| pH FEED | | | | | | | | | | | |
| DIST. | | | | | | | | | | | |
| CONC. | | | | | | | | | | | |
| POND BC | | | | | | | | | | | |
| CONDUCTIVITY FEED | | | | | | | | | | | |
| DIST. | | | | | | | | | | | |
| CONC. | | | | | | | | | | | |
| pH FEED | | | | | | | | | | | |
| DIST. | | | | | | | | | | | |
| CONC. | | | | | | | | | | | |
| POND BS | | | | | | | | | | | |
| CONDUCTIVITY FEED | | | | | | | | | | | |
| DIST. | | | | | | | | | | | |
| CONC. | | | | | | | | | | | |
| pH FEED | | | | | | | | | | | |
| DIST. | | | | | | | | | | | |
| CONC. | | | | | | | | | | | |

Rocky Flats, P.I.

9/13/90

RICHARD W. BOOTH

| TIME | 700 | 800 | 830 | 900 | 930 | 1000 | 1030 | 1100 | 1130 | 1200 | 1230 |
|--------------------------------------|------|------|------|------|------|------|------|------|------|------|------|
| VC FEED PH | - | 9.4 | 8.9 | 8.8 | 9.1 | 9.1 | 9.0 | 9.0 | 8.9 | 8.9 | 8.9 |
| FLASH DIST/COND. $\mu\text{s/cm}$ | 27.6 | 31.3 | - | 23.3 | 17.7 | 15.9 | 11.1 | 11.1 | 7.1 | 5.5 | 5.4 |
| FLASH DIST/PH | - | 9.0 | - | 7.4 | 7.2 | 7.8 | 7.9 | 8.4 | 7.9 | 7.5 | 7.1 |
| VC DIST /COND. $\mu\text{s/cm}$ | 58.7 | 54.6 | - | 34.9 | 38.9 | 37.0 | 39.3 | 46.3 | 43.8 | 47.1 | 48.5 |
| VC DIST/PH | - | 9.4 | 8.9 | 8.8 | 7.1 | 7.4 | 7.4 | 7.7 | 7.7 | 7.3 | 7.3 |
| DIST/COMBINED COND. $\mu\text{s/cm}$ | 40.0 | 64.0 | 53.0 | 61.0 | 56.5 | 64.0 | 76.1 | 64.8 | 50.0 | 52.5 | 51.5 |
| DIST/COMBINED PH | - | - | 8.1 | 8.2 | 7.7 | 7.9 | 8.2 | 8.3 | 8.1 | 8.1 | 7.8 |
| FLASH CONC. PH | 9.2 | 9.4 | 8.5 | 8.2 | 8.6 | 8.7 | 8.7 | 8.7 | 8.7 | 8.7 | 8.7 |
| VC CONC. PH | 9.2 | 9.0 | 8.4 | 8.2 | 8.2 | 8.2 | 8.2 | 8.3 | 8.3 | 8.2 | 8.3 |

| TIME | 100 | 130 | * 200 | 230 | 300 | 330 | | | | | |
|---------------------|------|------|----------|------|------|-------|--|--|--|--|--|
| VC FEED PH | 8.8 | 8.8 | — | — | — | — | | | | | |
| FLASH DIST/COND. | 4.1 | 5.1 | 5.1 | 8.0 | 15.9 | 179.2 | | | | | |
| FLASH DIST/PH | 7.5 | 7.6 | 8.0 | 8.2 | 7.8 | 7.5 | | | | | |
| VC DIST /COND. | 48.6 | 47.7 | 44.3 | 41.9 | — | — | | | | | |
| VC DIST/PH | 7.1 | 7.1 | 7.4 | 7.4 | 7.4 | — | | | | | |
| DIST/COMBINED COND. | 46.2 | 51.3 | 21.8 | — | — | — | | | | | |
| DIST/COMBINED PH | 7.5 | 7.5 | 8.2 | 8.2 | 7.8 | 7.5 | | | | | |
| FLASH CONC. PH | 8.7 | 8.7 | 8.7 | 8.6 | 8.2 | 8.5 | | | | | |
| VC CONC. PH | 8.3 | 8.2 | 8.2 | 8.3 | — | — | | | | | |

* Change over from VC to 4th stage of Flash Unit
 Combined Distillate conductivity down due to reduced flow/cut back to 1/391

APPENDIX 'D'

TABLE 1 SUMMARY OF ANALYSIS BY ANALYTIC TECHNOLOGIES (1)

Performed on water samples taken on September 13, 1990
compared to ChemTreat Analysis done by Rob Farrell on October 2, 1990 (2)

| PARAMETER | FEED (1) | FEED (2) | DIST (1) | DIST (2) | CONC (1) | CONC (2) | FILTERED (2) |
|-----------------------------------|----------|----------|----------|----------|----------|----------|--------------|
| P ALKALINITY | - | 3 | - | 0 | - | 0 | - |
| M ALKALINITY | 128 * | 47 * | 19 | 17 | - | 179 * | 50 |
| TOTAL HARDNESS | - | 403 | - | 3.9 | - | 1444 | 1454 |
| pH | 9.01 | 8.86 | 7.24 | 7.27 | 8.78 | 8.33 | - |
| CALCIUM | 81 | 79 | BDL | 1 | 165 | 297 | 290 |
| CARBONATE | 11 * | - | BDL | - | 3 * | - | - |
| CHLORIDE | 2387 | 374 | 2 | - | 829 | 1024 | - |
| POTASSIUM | 307 | - | 2 | - | 1000 | - | - |
| MAGNESIUM | 88 | 324 * | 0.62 | 2.9 * | 305 | 1147 * | 1167 * |
| NITROGEN (NITRATE) | 164 | - | 1.1 | - | 500 | - | - |
| SODIUM | 218 | - | 1.9 | - | 800 | - | - |
| SULPHATE | 496 | - | 4 | - | 1211 | - | - |
| TDS | 1898 | - | 12 | - | 6706 | - | - |
| SS | 3197 | - | - | - | 23 | - | - |
| CONDUCTIVITY (MS) MICROSIEMENS | - | 2300 | - | 4.1 | - | - | - |

* as CaCO₃

TEST NO. 2, September 14 and 15 1990

Summarizing the attached detailed test report, Appendix 'D'; it turned out that a very fortunate error was made in mixing the chemicals. The calcium and sodium amounts got switched and we actually handled fifteen times the amount of calcium that had been estimated for the ponds. Since the calcium has much lower solubility than sodium, this error furnished some very valuable information during the test.

We first noticed that the distillate water purity was to say the least, unacceptable and the rate of scaling on the heat transfer surfaces was alarming. We found that acid would remove the scale and the evolution of CO_2 indicated CaCO_3 scale, common in sea water evaporators and easily controlled by acid injection.

It was decided to continue the test on the remaining water using acid injection, as is done in sea water distillation. Again, fortunately the only acid we had in enough quantity was EDTA (HAMP-ENE ACID) or ethylenediaminetetraacetic acid. This acid was added at a rate of eight pounds per thousand gallons with the following unexpected results (serendipity).

1. The milky solution in all tanks became crystal clear
2. The VC distillate conductance fell rapidly from 350 MS (microsiemens) on the previous run without the acid, down to less than 10 MS.
3. The alkaline scale that had been deposited on the VC heat transfer surfaces was, as expected, being rapidly dissolved by the acidic conditions.

Rob Farrell of ChemTreat said he had observed similar phenomena as observation No. 2 in his feed treatment of boilers. When the alkalinity is reduced, he had noticed an improvement in steam quality but not to the remarkable degree observed here.

TEST NO. 3, September 24, 25 and 26 1990
See Appendix 'E' for Log Sheets

In order to attain a high enough concentration ratio it was decided to employ both storage tanks for a total of 2800 gallons and evaporate this quantity down as low as possible from mixture of the following chemicals per 1400 gallons:

| | |
|--------------------|----------------|
| Calcium Nitrate | 3.5 lb |
| Sodium bicarbonate | 7.0 lb |
| Potassium Chloride | 28.0 lb |
| Sodium Carbonate | 10.5 lb |
| Sodium Nitrate | 53.2 lb |
| Magnesium Sulphate | <u>42.0 lb</u> |
| | 144.2 lb |

Initial testing started 24 September 1990 at 1000 hr. with above solution having a resultant pH of 9.7. Scale started to form on the VC heating bundle so we added 0.5 lb. EDTA to VC concentrate tank at 1200 hr. bringing pH down to 6.5 and bundle started to clean - pH was back to 8.5 at 1230 so we added another 0.5 lb. and brought pH back to 6.5. This demonstrated feasibility of cleaning while operating. Notice that delta T of compressor fell from 17° to 15° (T6-T5) after acidification and resultant cleaning. We shut down at 1310 awaiting arrival of E G & G engineers.

With E G & G engineers present we restarted the next day, the 25th at 1430 after adding 5 lb. of EDTA to 650 gallons remaining in tank No. 1 making a total of 6 lb. added to the original 1400 gallons and ran until 1830, when supply from tank 1 was exhausted.

Restarted the next day, the 26th at 1000 hr. after adding 9 lb. EDTA to 1400 gallons in tank 2, bringing the pH down from 9.7 to 8.1 but feed averaged 8.6 and gradually rose to 9.0 indicating poor mixing or a reaction in the tank. Operation continued until 2045 hr. when the entire 1400 gallons was processed and the VC could no longer operate because of low level in the VC concentrate tank. One of the readings that had plague us was the fact that the combined distillate readings were always higher than the individual readings from both the VC and the MEMS - we finally discovered at 1400 hr. that a drain line from the VC concentrate tank had a minute leak into the combined distillate line which we fixed and the combined dropped from 150 to 40 microsiemens with 30 in the VC. As the concentration increased, the VC rose to 70 and the combined was 70 with the flash at 10 microsiemens. Lower alkalinity would probably have improved the VC distillate but these readings were within specifications. The VC was shut down at 2040 hr. and its residue was blown down to the MEMS which continued to operate until 2100 hr. The conductivity of the supernatant by dilution ratio was 222,800 MS. on shutdown with an estimated residue of about 150 gallons in the system.

TEST NO. 4, September 27 1990

In order to attain still higher concentration some minor piping changes to the MEMS enabled us to drain the top two stages into the third and fourth stage concentrate tanks. We rigged the second stage eductor to a separate tank so that we could still monitor distillate quality at higher concentrations in the fourth stage flash.

The test was continued at 1200 hr. and the concentrate from the 2800 gallons was dewatered down to 85.44 gallons by 1500 hr. - a volume reduction of 32.75 to 1. The next day Rob Farrell checked the chloride ratio at 27.57 to 1. Some concentrate may have been lost in the transfer and we may have lost some Chloride. The concentrate in the fourth stage, again by dilution ratio, was 390,000 microsiemens and if we use the 0.825 factor we arrive at 320,000 ppm - a pretty good check. Also the ratio of Test No. 1 feed with 25.4 lb. of chemicals added provided TDS of 1898 and conductivity of 2300 MS would extrapolate with 144.2 lb. for test 3 to 10,775 ppm and 13,057 microsiemens - by proportionating, we calculated 13,600. If we average this at 13,330 MS and ratio it to 390,000 we have 29.25 - another good check $10,775 \times 29.25 = 315,000$ ppm. It should be safe to assume the concentrate was in the range of 300,000 ppm based on 10,000 ppm feed. There was still no great amount of precipitation and most important the supernatant was still pumpable. Table 2 lists the data recorded.

TEST NO. 5, October 1 1990

Since the concentrate was still pumpable we made some more piping changes to allow operating only the fourth stage of the MEMS with the 85 gallons of concentrate in the 4th stage tank. We expected some dramatic results to happen very quickly so we did not bother with taking logs. The following data was collected while evaporating at a rate of about 15 GPH.

| | <u>Dist. Cond.</u> | <u>Dist. pH</u> | <u>Conc. pH</u> | <u>Conc. Cond.</u> |
|--------|--------------------|-----------------|-----------------|--------------------|
| Start | 17 MS | | 7.9 | 390,000 MS |
| | 9 MS | 9.1 | 7.3 | 587,000 MS |
| | 21 MS | 8.6 | 6.6 | 789,000 MS |
| Finish | 36 MS | 8.5 | 6.6 | 1,055,000 MS |

TABLE 2 DATA RECORDED FOR TEST 4

SEPTEMBER 27, 1990

| TIME | 1200 | 1230 | 1300 | 1330 | 1400 | 1430 | 1500 |
|-----------------|---------|------|---------|------|---------|-------|---------|
| 3rd Stage pH | 8.6 | 8.3 | 8.3 | 8.2 | 8.2 | 8.2 | 8.1 |
| MS/cm-Cond | 157,500 | | 178,920 | | 212,520 | | 241,500 |
| 4th Stage pH | 8.4 | 8.3 | 8.2 | 8.1 | 8.1 | 8.0 | 7.9 |
| MS/cm-Cond | 228,480 | | 261,030 | | 286,860 | | 389,760 |
| Dist. pH | 9.9 | 8.8 | 7.7 | 7.2 | 7.5 | 7.3 | 6.7 |
| MS/cm-Cond | 0.53 | 0.12 | 0.06 | 0.02 | 0.07 | ±0.12 | 0.017 |
| 3rd Stage Ratio | 12:1 | | 13.64:1 | | 16.20:1 | | 18.5:1 |
| 4th Stage Ratio | 17.5:1 | | 19.89:1 | | 21.86:1 | | 30:1 |

Concentrate left in 4th stage tank -- 85.44 Gallon residue

We were amazed how well the salts remained in solution or in fine suspension up to 800,000 MS but then the solution started to precipitate and we had to shut down. The supernatant was proportioned to be about one million microsiemens. The final volume was 20 gallons plus some lost in transfer.

Test No. 4 provided the criteria for immediately estimating results

Safe operation at 650,000 ppm

Maximum obtainable 825,000 ppm

Concentration Ratio w/10,000 ppm feed

Safe at $\frac{650,000}{10,775} = 60$ to 1 ppm

Maximum $\frac{1,055,000}{13,300} = 80$ to 1 cond.

Weight Analysis: The 20 gallons of concentrate weighed 256 pounds or a specific gravity of 1.5. Since 142.2 lb. of chemicals were added, the balance must be free water and or water of hydration. Weight wise the ratio is 90 to 1.

CONCLUSIONS AND RECOMMENDATIONS

Supplementing the Executive Summary, it is reasonable to conclude the following from the tests provided the synthetic pond water closely approximates actual conditions.

1. Control of alkalinity is vital from the standpoint of acquiring high purity distillate and the elimination of alkaline scales such as calcium carbonate and magnesium hydroxide. EDTA is recommended at a rate of at least 6 lb. per 1000 gallons but this rate may be reduced with the use of polymers which will involve field testing to optimize minimum injection rate.
2. If scaling or distillate impurity should occur the EDTA can be increased during operation. The second stage MEMS eductor will handle any gassing of CO₂ from the chemical reactions..
3. The EDTA evidently also aids in tying up the calcium and magnesium ions to prevent precipitation and allows concentration to proceed safely to as high as 60%. Further dewatering or drying can be accomplished with a pot dryer using additional heat from the engines by water washing the stack gases. If this is of interest please advise.
4. It can also be concluded that should other sites involve high calcium content these too can be handled but the concentration ratio may not be as high because of the lower solubility of calcium. Concentrate samples from test No. 2 has been saved for your chemical analysis, should you desire to investigate this further.
5. Modified test runs were made possible by eliminating the cost of needless chemical analysis. Simpler mechanical methods

that proved more fool proof were developed to quickly determine the concentration ratios and distillate purity. Samples have been saved and we recommend that your own laboratory do any chemical analysis you may require. If so, please advise shipping instructions - all together the volume of samples and ~~concentrate~~^{concentrate} is about 50 gallons. The concentrates in particular may prove valuable for establishing cementing techniques.

APPENDIX 'A'

LICON EVAPORATOR TEST REQUIREMENTS

VC50 in series with Memms 204

1. Test Time

Four tests of 12 hours each, totaling 48 hours. These tests will be run September 12 through September 14.

2. Test Mode

One test for each type of feed (Each type of feed must simulate the pond water of Pond 207A or Pond 207B North or centre or South). Feed rate for each test shall be ~~1.25 gpm normal up to 2 gpm maximum.~~

2.25 ± 0.25 gpm

3. Sampling Frequency

A feed sample shall be collected at the beginning of each test. Composite samples of distillate and concentrate stream shall be collected for each test and shall be made up by a series of four ounces sub-samples collected every 30 min.

4. Sample Distribution

polypropylene

All sub-samples shall be collected in a ~~glass~~ jar large enough, to hold 3/4 of a gallon in volume. Each composite sample shall be divided into two equal parts. One part is for LICON's analysis, the other part will be sent to Rocky Flats for references. All samples shall be placed in glass jars with teflon lined lids and clearly labeled.

| <u>Sample total</u> | <u>LICON</u> | <u>Rocky Flats</u> |
|-----------------------|--------------|--------------------|
| Feed | 4 | 4 |
| Composite Distillate | 4 | 4 |
| Composite Concentrate | 4 | 4 |

5. Process Readings

Conductivity, temperature, pressure, power input and output, and flow rate of feed and discharge, shall be recorded every 30 min. while tests are being run. Test summary report shall indicate the length of time to start up each system, at what point steady state was achieved, and intermitten changes of flow rate.

6. Analysis

Each sample taken from the feed, distillate, and concentration shall be analyzed for the following compounds.

| <u>Feed</u> | <u>Distillate</u> | <u>Concentrate</u> |
|-------------|-------------------|--------------------|
| Alkalinity | Alkalinity | - |
| Carbonate | Carbonate | Carbonate |
| Nitrate | Nitrate | Nitrate |
| Sulfate | Sulfate | Sulfate |
| TDS | TDS | TDS |
| Calcium | Calcium | Calcium |
| Magnesium | Magnesium | Magnesium |
| Potassium | Potassium | Potassium |
| Sodium | Sodium | Sodium |
| pH | pH | pH |
| TSS | - | TSS |

7. Feed Stream Preparation

Four types of waste water shall be prepared by LICON to simulate each of the four ponds at the Rocky Flats Plant. The Feed Stream shall be mixed continuously for a minimum of 8 hours prior to test and shall be mixed in feed tank during the test.

Each feed stream shall be prepared as follows:

To tap water add the following chemicals in the amount shown.

| <u>Chemicals</u> | <u>Lbs/1000 Gals of Water</u> | | | |
|--|-------------------------------|-------|-------|-------|
| | Pond A | BN | BC | BS |
| Calcium Nitrate ($\text{Ca}(\text{NO}_3)_2 \cdot 3\text{H}_2\text{O}$) | 2.5lb | 7.5 | .8 | 1.1 |
| Magnesium bicarbonate (MgHCO_3) | 2.7lb | 2.5 | 4.1 | 4.1 |
| Potassium Chloride (KCl) | 4.1 | 1.1 | 9.1 | 10.5 |
| Sodium Carbonate ($\text{Na}_2\text{CO}_3 \cdot \text{H}_2\text{O}$) | .1 | 5.2 | 4.7 | 1.1 |
| Sodium Nitrate (NaNO_3) | 4.2 | 10.4 | 16.8 | 8.7 |
| Sodium Sulfate ($\text{Na}_2\text{SO}_4 \cdot 7\text{H}_2\text{O}$) | 4.2 | 13.7 | 15.9 | 7.7 |
| Sodium Chloride (NaCl) | - | 4.8 | - | - |
| pH | 10-11 | 10-11 | 10-11 | 10-11 |

All pH adjustments shall be made with sodium hydroxide or hydrochloric acid.

Disposal of waste water shall be the responsibility of LICON.

8. Deliverables

Complete test equipment set up diagram and data form shall be delivered a minimum of 3 days prior to test for approval.

Final report shall be delivered 3 working days following the completion of test activities.

The final report shall include:

- 1) brief system description
- 2) observations
- 3) collected data
(i.e. conductivity, temperature, pressure, and flow rate)
- 4) analytical results
- 5) conclusions

9. Test Observations

Rocky Flats personnel will observe at least one test start up and one test completion.

APPENDIX 'B'

PROCEDURE FOR TESTING POND WATER SIMULATION
AT ROCKY FLATS PER JOB ORDER
EMPLOYING LICON'S VC 90 AND MEMS 204

TEST NO. 1 Pond A Water $17.8/8333 \times 10^6 = 2136$ ppm

Run both plants at design conditions, 175-180°F suction temperature in VC (T5) and 180-185°F top temperature (T23) when 1400 gallon tank is empty - shut down VC plant. Run MEMS until VC shell and tank are drained and continue running MEMS until Flash Chambers and tanks 3 and 4 are at lowest level possible. Shut down MEMS and drain all residue to collector tank.

TEST NO. 2 Pond BC Water $51.4/8333 \times 10^6 = 6168$ ppm

Same as above.

TEST NO. 3 Pond BS Water $33.2/8333 \times 10^6 = 3984$ ppm

Same as above.

TEST NO. 4 Pond BN Water $45.2/8333 \times 10^6 = 5424$ ppm

Run same as Test 1 except pump residue in stages 1 and 2 to tanks 3 and 4.

TEST NO. 5 Degree of Concentration Attainable

Repipe MEMS to use city water as feed to stages 1 and 2. Start MEMS using concentrate from collector tank to feed stage 3 tank and run until precipitation occurs in either or both tanks, 3 and 4.

APPENDIX 'C'

SEPTEMBER 20, 1990

**ROCKY FLATS SYNTHETIC POND 'BC' WATER
TEST NO.2, JOB 901**Summary of Test Results, Conclusion and Projections

The modifications to the test procedure outlined in the previous report were helpful, enabling a smoother start up as evidenced by the attached log sheets taken 14 September 1990. The first disappointment was the poor quality of the VC product water which ranged 40 to 50 micro siemens during Test No. 1 was now ranging as high as 600 at the start and gradually dropped to 350 micro siemens. The natural conclusion was to condemn the new mesh.

A more serious situation however was developing with the MEMS- the recirculation rate around the top two stages was dropping rapidly from 40 GPM to 18 GPM in two hours of running. A sludge had been noticed forming in the first test and was forming much more rapidly in this test. The natural assumption was that this sludge was blocking the tubes in the heater. A shut down became necessary after the 1100 reading.

When the heater bundle was removed, we found a very heavy deposit of scale which was effectively removed by flooding the bayonet tubes with dilute 5% HCl. The reaction generated a large amount of frothing indicated the release of CO₂ and identifying calcium carbonate - an alkaline scale common in sea water evaporators and easily controlled by acid injection.

Since there was still 600 gallons in the storage tank we decided to try acid injection. Fortunately we did not have enough HCl but we did have a considerable quantity of EDTA (HAMP-ENE ACID) which should tie up the calcium. We calculated we would need 8 lb. to treat 1000 gallons.

The next day we added 4.8 lb of this acid to the remaining 600 gallons; 4.6 oz. in the VC tank; 1.0 lb. to the 3rd stage MEMS tank and 0.6 lb. in the 4th stage tank. The milky solution in all tanks became crystal clear with addition of the EDTA. Test No. 2 was restarted at 0738 September 15, 1990 and we soon became aware that the distillate conductance was falling rapidly from a low of 350 micro siemens at the end of the previous aborted run. When the VC got up to operating temperatures and capacity at 0830 the sample pot was down to 33 micro siemen and the tank, 108 micro siemen - by 1030 8 and 10. We actually recorded as low as 5 in the VC pot and 6.3 in the VC tank at shut-down 1320. The slight amount of scale that had formed on the tubes of the VC dissolved as did scale on the shell.

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The pH of the feed ranged at start from 3.3 rising to 4.4 at 1230. The pH of the VC distillate averaged about 4 due to CO_2 pick up from the breakdown of the HCO_3 to CO_2 with acid injection. The distillate from the fourth stage flash² sample pot in the eductor suction ranged from 20 to 35 micro siemens and its pH was alkaline ranging from 8.7 to 9.2 since all of the CO_2 had been stripped in the VC.

The first results from Pioneer Laboratory indicated that the VC tank precipitate was principally calcium carbonate and since we already suspected the scale in the heater bundle was calcium carbonate we wondered where all the calcium was coming from? A check of the remaining chemicals soon established that a mistake had been made in that calcium nitrate and the sodium nitrate quantities had been reversed 53.2 lb. vs 3.5 lb. This test is therefore invalidated but it certainly taught us some valuable lessons about the chemistry, particularly the effect of alkalinity on water purity. It also revealed that we could attain the desired concentration ratio under the most adverse conditions. Because of the finite feed we employed the technic of operating the MEMS unit with city water in the upper stages - in this case the three top stages and modifications in the fourth stage concentrate tank permitted the residue to be reduced to 46 gallons, or with two stages as in Test No. 1 to 104 gallons. By simple arithmetic if we wanted to attain say 360,000 ppm from 12,000 ppm feed we would need a supply of $104 \times 360,000/12,000 = 3120$ gallons based on final two stage operation; and $46 \times 360,000/12,000 = 1380$ gallon of feed stock based on 46 gallons of residue and single stage operation.

Now that we have to repeat the test it would behoove us to mix up the chemicals previously listed into both tanks (2800 gallons). At start-up, both the VC and the MEMS should be fed in parallel for the first two hours, at which time the VC will have stabilized at about 24,000 ppm i.e.

At start up the VC has 150 gallons of 12,000 ppm solution in the system and in the first two hours will evaporate about 3/4 its normal rate of 100 GPH or 150 gallons so 300 gallons of feed will be reduced to 150 gallons at twice the feed concentration. From here on the two plants will be fed in series at a rate of about 150 GPH; with the VC evaporating 90 GPH the concentrate will then stabilize at 30,000 ppm, and remain at this concentration for the balance of the test blowing down the 60 GPH and 30,000 ppm to the MEMS.

After operating to reduce the 2800 gallons to 400 gallons residue in $2400/150 = 16$ hr. the VC must be shut down and the MEMS must continue to operate until the 150 gallons (about 2 hr.) from the VC is evaporated and then the concentrate of the MEMS residue (250 gallons) will average 134,400 ppm. The MEMS must then be shut down and the top two stages drained to the third and fourth stage tanks. Operation can then continue until the residue in the two tanks and both stages are reduced to 104 gallons (the minimum to

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keep pumps operating) and then the residue will average 323,000 ppm. If further concentration appears possible then the MEMS can be shut down again; the third stage and tank drained to fourth stage tank. The third stage can be rigged to operate on city water and the test continued down to 46 gallons where massive precipitation should occur.

In summary we would like to reiterate that this type of testing is not R & D as we understand is the interpretation at R.F. Feed stocks vary so widely at different sites that Licon makes their test units available to the potential customer so that the chemistry can be analyzed before field testing. Field testing is still necessary if the feed stock varies but these shop test provide valuable data for quickly optimizing the pretreatment necessary to get the best quality of distillate and the maximum concentration ratio. The adjustments that had to made to the plants were made purely to get maximum data from limited feed stock since we will have to store the sludge and probably dry it to dispose of it.

 9/24

| | | | | | | | | | | |
|-------------------|---------|-------|-------|--------|-------|-------|-------|-------|-------|--|
| DATE: | 5/14/90 | | | | | | | | | |
| TIME: | 7:30 | 8:00 | 8:30 | 9:00 | 9:30 | 10:00 | 10:30 | 11:00 | 11:30 | |
| POND A | | | | | | | | | | |
| CONDUCTIVITY FEED | | | | | | | | | | |
| DIST. | | | | | | | | | | |
| CONC. | | | | | | | | | | |
| pH | | | | | | | | | | |
| FEED | | | | | | | | | | |
| DIST. | | | | | | | | | | |
| CONC. | | | | | | | | | | |
| POND BN | | | | | | | | | | |
| CONDUCTIVITY FEED | 10.64 | 10.67 | 10.72 | 10.65 | 10.65 | | | | | |
| Com R. DIST. #4 | 0.66 | 0.89 | 0.93 | 0.64 | 0.63 | | | | | |
| CONC. #6 | - | - | | 23000+ | 16.49 | | | | | |
| pH | | | | | | | | | | |
| FEED #4 | 7.5 | 7.6 | 7.6 | 7.6 | 7.7 | | | | | |
| Com B. DIST. #5 | 7.4 | 7.3 | 7.5 | 7.8 | 8.0 | | | | | |
| CONC. #6 | | | | 8.1 | 7.8 | | | | | |
| POND BC | | | | | | | | | | |
| CONDUCTIVITY FEED | | | | | | | | | | |
| DIST. | | | | | | | | | | |
| CONC. | | | | | | | | | | |
| pH | | | | | | | | | | |
| FEED | | | | | | | | | | |
| DIST. | | | | | | | | | | |
| CONC. | | | | | | | | | | |
| POND BS | | | | | | | | | | |
| CONDUCTIVITY FEED | | | | | | | | | | |
| DIST. | | | | | | | | | | |
| CONC. | | | | | | | | | | |
| pH | | | | | | | | | | |
| FEED | | | | | | | | | | |
| DIST. | | | | | | | | | | |
| CONC. | | | | | | | | | | |

Start Compresses at 6:35. went down low water at 6:50. Start Back up. Took sample at Top Tank before start up. Conduct/ 10.61 "C/F. J pH 7.5. done flush off until V.C. is up to Temp.

Rocky Flats, Col.

9/14/90

RICHARD W. BOOTHE

| TIME | 720 | 730 | 800 | 830 | 900 | 930 | 1000 | 1030 | 1100 | 1130 | 1200 |
|---------------------------|------------------------|------------------------|------------------------|------------------------|-------------------------|------------------------|------------------------|-------------------------|-------------------------|------|------|
| #4 VC FEED PH | 7.5 | 7.5 | 7.6 | 7.6 | 7.6 | 7.7 | 8.1 | 8.1 | 9.6 | | |
| FLASH DIST/COND. | | 0.71 ^{ms/cm} | 0.71 ^{ms/cm} | 0.77 ^{ms/cm} | 0.57 ^{ms/cm} | 0.57 ^{ms/cm} | 0.38 ^{ms/cm} | 0.33 ^{ms/cm} | 0.23 ^{ms/cm} | | |
| FLASH DIST/PH | | 7.6 | 7.6 | 7.6 | 8.2 | 7.9 | 8.1 | 8.3 | 8.5 | | |
| VC DIST /COND. | | 0.55 ^{ms/cm} | 0.57 ^{ms/cm} | 0.59 ^{ms/cm} | 0.50 ^{ms/cm} | 0.47 ^{ms/cm} | 0.32 ^{ms/cm} | 0.37 ^{ms/cm} | 0.15 ^{ms/cm} | | |
| VC DIST/PH | | 7.0 | 6.9 | 6.9 | 7.1 | 7.2 | 7.9 | 7.8 | 8.4 | | |
| #5 DIST/COMBINED COND. | | 0.66 ^{ms/cm} | 0.59 ^{ms/cm} | 0.93 ^{ms/cm} | 0.64 ^{ms/cm} | 0.63 ^{ms/cm} | 0.47 ^{ms/cm} | 0.67 ^{ms/cm} | 0.02 ^{ms/cm} | | |
| #5 DIST/COMBINED PH | | 7.4 | 7.3 | 7.5 | 7.8 | 9.0 | 8.5 | 8.9 | 8.9 | | |
| #6 FLASH CONC. PH | | | | | 8.1 | 7.9 | 7.8 | 7.7 | 7.9 | | |
| VC CONC. PH | | 7.5 | 7.5 | 7.5 | 7.4 | 7.4 | 7.5 | 7.5 | 7.8 | | |
| #4 (TANK) Feed Conduct. | 10.64 ^{ms/cm} | 10.64 ^{ms/cm} | 10.67 ^{ms/cm} | 10.72 ^{ms/cm} | 10.65 ^{ms/cm} | 10.65 ^{ms/cm} | 10.57 ^{ms/cm} | 10.62 ^{ms/cm} | 10.53 ^{ms/cm} | | |
| #6 - FLASH CONC. Conduct. | ms/cm | | | | 20000+ ^{ms/cm} | 16.49 ^{ms/cm} | 19.56 ^{ms/cm} | 20000+ ^{ms/cm} | 20000+ ^{ms/cm} | | |

Note: Combined Dist readings until 900 were only VC distillate. 900 readings include Flash Distillate

Note: 9:35 caustic added to feed Tank / raise PH

Note: 10:40 caustic added to Feed Tank

CTT DIST/COND OUT

| | |
|-----|------------|
| PH | Cond |
| 7.3 | 0.44 ms/cm |
| 8.3 | 0.46 |
| 9.3 | 0.46 |
| 30 | |
| 100 | |
| 130 | |

POND WATER *BW*

DATE: 9-15-7

| TIME: | 8:30 | 9:00 | 9:30 | 10:00 | 10:30 | 11:00 | 11:30 | 12:00 | 12:30 |
|----------------------------|--------|--------|--------|--------|--------|--------|--------|--------|-------|
| TEMPERATURES: | | | | | | | | | |
| T1 FEED SUPPLY | 91 | 92 | 92 | 92 | 91 | 94 | 94 | 94 | 94 |
| T2 FEED TO VC | 149 | 169 | 756 | 144 | 143 | 131 | 160 | 148 | 138 |
| T3 VC RECYCLE FEED | 186 | 186 | 178 | 187 | 183 | 173 | 188 | 166 | 183 |
| T4 BLOWDOWN TO MEMS | 82 | 102 | 160 | 168 | 169 | 166 | 164 | 169 | 167 |
| T5 VC SUCTION | 175 | 176 | 175 | 177 | 176 | 170 | 176 | 175 | 176 |
| T6 VC VENT | 195 | 198 | 195 | 198 | 195 | 188 | 196 | 192 | 194 |
| T7 VC CHEST | 198 | 200 | 197 | 200 | 198 | 190 | 198 | 194 | 192 |
| T8 VC EDUCTOR DISCH. | 182 | 189 | 185 | 189 | 187 | 184 | 184 | 181 | 183 |
| T9 VC DISTILLATE IN HX | 166 | 180 | 172 | 173 | 174 | 176 | 179 | 167 | 172 |
| T10 VC DIST. OUT HX | 116 | 116 | 109 | 106 | 105 | 105 | 118 | 116 | 106 |
| T11 1ST FLASH VAPOR | n | n | 180 | 170 | 163 | 131 | 160 | 168 | 166 |
| T12 2ND FLASH VAPOR | | | 168 | 158 | 155 | 131 | 150 | 156 | 156 |
| T13 3RD FLASH VAPOR | | | 135 | 136 | 133 | 124 | 126 | 127 | 129 |
| T14 4TH FLASH VAPOR | | | 120 | 120 | 117 | 121 | 111 | 111 | 111 |
| T15 COOLANT INLET | | | | 105 | 103 | 96 | 100 | 100 | |
| T16 COOLANT OUTLET | | | 111 | 117 | 111 | 93 | 108 | 108 | 107 |
| T17 4TH FLASH CONC. | | | 117 | 120 | 116 | 120 | 112 | 117 | 112 |
| T18 4TH FLASH FEED | | | 129 | 131 | 126 | 121 | 122 | 122 | 122 |
| T19 3RD FLASH CONC. | | | 140 | 144 | 140 | 131 | 135 | 135 | 131 |
| T20 3RD FLASH FEED | | | 160 | 155 | 150 | 127 | 145 | 146 | 145 |
| T21 2ND FLASH CONC. | | | 145 | 158 | 150 | 125 | 149 | 155 | 156 |
| T22 FEED TO HTR. | | | 176 | 162 | 154 | 123 | 151 | 158 | 148 |
| T23 OUTPUT FROM HTR. | | | 170 | 161 | 153 | 115 | 150 | 157 | 155 |
| F1 FIRST STAGE RECYCLE | 40 GPM | 40 GPM | 40 GPM | 46 GPM | 40 |
| F2 VC FEED RATE | 2 | 2 | 2 3/4 | 2.45 | 2.3 | 3.0 | 2 | 3 | 3 |
| F3 VC BLOWDOWN | 0 | 0 | .8 | .8 | 0 | 1.0 | .8 | 1.0 | 1.0 |
| F4 VC RECYCLE | 3 | 3 | 2 3/4 | 3 | 2 3/4 | 3.1 | 2 3/4 | 2 3/4 | 3" |
| H1 VC BRINE WEIR | 1" | 1" | 1" | 1 1/4" | 1 1/4" | 1" | 1" | 1" | 1" |
| H2 3RD STAGE WEIR | — | — | 3" | 3" | 3" | 3" | 3" | 3" | 3" |
| H3 4TH STAGE WEIR | — | — | 3" | 3" | 3" | 3" | 3" | 3" | 3" |
| FEED TANK LEVEL <i>675</i> | 625 | 575 | 500 | 475 | 350 | 275 | 200 | 150 | 100 |
| M1 VC DISTILLATE | 1609 | 1655 | 1703 | 1753 | 1709 | 1743 | 1900 | 1954 | 1923 |
| M2 MEMS DISTILLATE | 1696 | 1672 | 1675 | 1675 | 1684 | 1684 | 1689 | 1694 | 1697 |
| M3 COMBINED DIST. | | 46 | 74 | 103 | 92 | 63 | 86 | 79 | 42 |
| V VOLTAGE | 475 | | 475 | 475 | 475 | 475 | 475 | 475 | 475 |
| A AMPS | 61.5 | | 60.5 | 59.2 | 57.5 | 58.2 | 38.1 | 56 | 57 |
| KW KILOWATTS | | | | | | | | | |
| PF POWER FACTOR | .52 | | .55 | .85 | .75 | .85 | .77 | .75 | .75 |

LOG SHEET FOR WATER SAMPLES

JOB ORDER 901

| | | | | | | | | | | | |
|-------------------|---------|-------|--------|--------|--------|--------|--------|--------|--------|------|--|
| DATE: | 9/15/90 | | | | | | | | | | |
| TIME: | 8:30 | 9:00 | 9:30 | 10:00 | 10:30 | 11:00 | 11:30 | 12:00 | 12:30 | 1:00 | |
| POND A | | | | | | | | | | | |
| CONDUCTIVITY FEED | | | | | | | | | | | |
| DIST. | | | | | | | | | | | |
| CONC. | | | | | | | | | | | |
| pH FEED | | | | | | | | | | | |
| DIST. | | | | | | | | | | | |
| CONC. | | | | | | | | | | | |
| POND BN | | | | | | | | | | | |
| CONDUCTIVITY FEED | 11.01 | 10.72 | 10.94 | 10.58 | 10.90 | 10.81 | 10.80 | 10.25 | 10.90 | | |
| DIST. | 1.57 | 147.5 | 0.21 | 0.23 | 41.7 | 29.0 | 31.8 | 20.9 | 0.23 | | |
| CONC. | - | - | 20000+ | 20000+ | 20000+ | 20000+ | 20000+ | 20000+ | 20000+ | | |
| pH FEED | 3.3 | 3.4 | 3.4 | 3.6 | 3.5 | 3.6 | 3.8 | 3.8 | 4.1 | | |
| DIST. | 5.9 | 5.4 | 6.2 | 4.9 | 5.9 | 6.0 | 6.2 | 5.3 | 6.2 | | |
| CONC. | - | - | 7.0 | 7.5 | 7.3 | 7.3 | 7.2 | 7.2 | 7.1 | | |
| POND BC | | | | | | | | | | | |
| CONDUCTIVITY FEED | | | | | | | | | | | |
| DIST. | | | | | | | | | | | |
| CONC. | | | | | | | | | | | |
| pH FEED | | | | | | | | | | | |
| DIST. | | | | | | | | | | | |
| CONC. | | | | | | | | | | | |
| POND BS | | | | | | | | | | | |
| CONDUCTIVITY FEED | | | | | | | | | | | |
| DIST. | | | | | | | | | | | |
| CONC. | | | | | | | | | | | |
| pH FEED | | | | | | | | | | | |
| DIST. | | | | | | | | | | | |
| CONC. | | | | | | | | | | | |

Change Dist on 1+2 sl. Together at 12:00.
 3+4 sl. Together

LOG SHEET ON ROCKY FLATS POND WATER TESTS

POND WATER 3W

9/15/90

JOB NO. 9/17/90

DATE: 9-15-90

| TIME: | 1:00 | 1:30 | 10:30 | 11:30 | 2:00 | 2:30 | 3:00 | 2:30 |
|--------------------------|-------|-------|-------|-------|-------|-------|------|------|
| TEMPERATURES: | | | | | | | | |
| T1 FEED SUPPLY | 92 | | | | | | | |
| T2 FEED TO VC | 174 | | | | | | | |
| T3 VC RECYCLE FEED | 185 | | | | | | | |
| T4 BLOWDOWN TO MEMS | 156 | | | | | | | |
| T5 VC SUCTION | 176 | | | | | | | |
| T6 VC VENT | 198 | | | | | | | |
| T7 VC CHEST | 200 | | | | | | | |
| T8 VC EDUCTOR DISCH. | 186 | | | | | | | |
| T9 VC DISTILLATE IN HX | 173 | | | | | | | |
| T10 VC DIST. OUT HX | 101 | | | | | | | |
| T11 1ST FLASH VAPOR | 168 | | 184 | 178 | 174 | 178 | | |
| T12 2ND FLASH VAPOR | 156 | | 172 | 162 | 162 | 165 | | |
| T13 3RD FLASH VAPOR | 119 | | 139 | 133 | 136 | 133 | | |
| T14 4TH FLASH VAPOR | 102 | | 112 | 101 | 103 | 103 | | |
| T15 COOLANT INLET | 99 | | 107 | 87 | 90 | 88 | | |
| T16 COOLANT OUTLET | 101 | | 99 | 99 | 101 | 99 | | |
| T17 4TH FLASH CONC. | 100 | | 111 | 100 | 104 | 100 | | |
| T18 4TH FLASH FEED | 110 | | 131 | 123 | 126 | 122 | | |
| T19 3RD FLASH CONC. | 123 | | 145 | 137 | 145 | 136 | | |
| T20 3RD FLASH FEED | 132 | | 165 | 155 | 158 | 155 | | |
| T21 2ND FLASH CONC. | 155 | | 170 | 162 | 165 | 165 | | |
| T22 FEED TO HTR. | 156 | | 180 | 168 | 172 | 173 | | |
| T23 OUTPUT FROM HTR. | 158 | | 183 | 178 | 182 | 175 | | |
| F1 FIRST STAGE RECYCLE | 4061 | | 4061 | 4061 | 4061 | 4061 | | |
| F2 VC FEED RATE | 3 | | | | | | | |
| F3 VC BLOWDOWN | 1.0 | | | | | | | |
| F4 VC RECYCLE | 3 | | | | | | | |
| H1 VC BRINE WEIR | 1" | | | | | | | |
| H2 3RD STAGE WEIR | 3" | | 3" | 3" | 3" | 3" | | |
| H3 4TH STAGE WEIR | 3" | | 3" | 3" | 3" | 3" | | |
| FEED TANK LEVEL | | | | | | | | |
| M1 VC DISTILLATE 1982 | 2639 | | | | | | | |
| M2 MEMS DISTILLATE 11907 | 16921 | 16950 | 17051 | 17100 | 17123 | 17131 | | |
| M3 COMBINED DIST. | 70 | | | | 23 | 8 | | |
| V VOLTAGE | 47.5 | | | | | | | |
| A AMPS | 37 | | | | | | | |
| KW KILOWATTS | | | | | | | | |
| PF POWER FACTOR | .7 | | | | | | | |

Rocky Flats, Cal.

9/15/90

RICHARD W. BOOTH

| TIME | 8:30 | 9:00 | 9:30 | 10:00 | 10:30 | 11:00 | 11:30 | 12:00 | 12:30 | 1:00 | 1:30 |
|--|-------|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| #4 VC FEED PH | 3.3 | 3.4 | 3.4 | 3.6 | 3.5 | 3.6 | 3.8 | 3.8 | 4.4 | 7.8 | |
| FLASH DIST/COND. $\mu\text{s}/\text{cm}$ | 0.31 | 0.21 | 130.1 | 71.1 | 57.7 | 51.1 | 40.5 | 43.7 | 47.1 | 1.70 | 1.1 |
| FLASH DIST/PH | 7.7 | 6.0 | 6.8 | 6.9 | 6.5 | 6.7 | 6.8 | 7.0 | 7.1 | 7.2 | 7.6 |
| VC DIST /COND. $\mu\text{s}/\text{cm}$ | 53.3 | 17.1 | 15.2 | 9.9 | 7.1 | 13.0 | 6.8 | 6.3 | 6.8 | | |
| VC DIST/PH | 5.4 | 5.1 | 5.1 | 4.9 | 4.4 | 4.6 | 4.7 | 4.9 | 5.0 | 7.2 | |
| #5 DIST/COMBINED COND. $\mu\text{s}/\text{cm}$ | 1.02 | 147.3 | 0.21 | 0.23 | 9.7 | 38.0 | 31.8 | 208 | 0.23 | 0.26 | 1.1 |
| #5 DIST/COMBINED PH | 5.9 | 5.4 | 6.2 | 4.9 | 5.9 | 6.0 | 6.2 | 5.3 | 6.2 | 6.8 | 6.1 |
| #6 FLASH CONC. PH | | | 7.0 | 7.5 | 7.3 | 7.3 | 7.2 | 7.2 | 7.1 | 7.0 | 6.1 |
| VC CONC. PH | 5.5 | 7.4 | 4.1 | 3.7 | 3.7 | 3.7 | 3.6 | 3.7 | 3.8 | | |
| #4 (Tank) Feed Conductivity (ms/cm) | 11.01 | 10.82 | 10.86 | 10.88 | 10.90 | 10.84 | 10.80 | 10.85 | 10.90 | 10.97 | |
| #6 Flash Conc. Conductivity (ms/cm) | | | 20000+ | 20000+ | 20000+ | 20000+ | 20000+ | 20000+ | 20000+ | 20000+ | 20000+ |

| PH | Cond |
|-----|--------------------------------|
| 7.6 | 0.68 $\mu\text{s}/\text{cm}$ |
| 7.5 | 0.44 $\mu\text{s}/\text{cm}$ |
| 7.4 | 0.29 $\mu\text{s}/\text{cm}$ |
| 7.2 | 0.21 $\mu\text{s}/\text{cm}$ |
| 7.1 | 164.2 $\mu\text{s}/\text{cm}$ |
| 7.1 | 132.9 $\mu\text{s}/\text{cm}$ |
| 6.8 | 93.5 $\mu\text{s}/\text{cm}$ |
| 6.9 | 73.2 $\mu\text{s}/\text{cm}$ |
| 7.0 | 151.57 $\mu\text{s}/\text{cm}$ |
| 7.1 | 0.37 $\mu\text{s}/\text{cm}$ |

Dist from sample pot flash

| PH | Cond |
|-----|------------------------------|
| 8.7 | 30.9 $\mu\text{s}/\text{cm}$ |
| 8.9 | 35.4 $\mu\text{s}/\text{cm}$ |
| 9.0 | 34.5 $\mu\text{s}/\text{cm}$ |
| 8.8 | 17.5 $\mu\text{s}/\text{cm}$ |
| 9.2 | 17.9 $\mu\text{s}/\text{cm}$ |
| 9.1 | 18.5 $\mu\text{s}/\text{cm}$ |
| 9.1 | 25.6 $\mu\text{s}/\text{cm}$ |
| 8.8 | 75.4 $\mu\text{s}/\text{cm}$ |
| 8.7 | 23.7 $\mu\text{s}/\text{cm}$ |

Rocky Flats, Col. 9/15/90

RICHARD W. BOOTHE

| TIME | 2:00 | 2:30 | 3:00 | 3:30 | 4:00 | | | | | | |
|--|----------------------|------|------|------|------|--|--|--|--|--|--|
| VC FEED PH | | | | | | | | | | | |
| FLASH DIST/COND. | 1.03 ^{mg/L} | | | | | | | | | | |
| FLASH DIST/PH | 6.9 | | | | | | | | | | |
| VC DIST /COND. | | | | | | | | | | | |
| VC DIST/PH | | | | | | | | | | | |
| DIST/COMBINED COND. | 1.07 ^{mg/L} | | | | | | | | | | |
| DIST/COMBINED PH | 7.0 | | | | | | | | | | |
| FLASH CONC. PH | 6.1 | | | | | | | | | | |
| VC CONC. PH | | | | | | | | | | | |
| #4 (Tank) Feed Conductivity | | | | | | | | | | | |
| #6 Flash Conc. Conductivity $\mu\text{S/cm}$ | 23100+ | | | | | | | | | | |

Flash

Dist. Sample pot

PH

Cond

8.0

23.8 $\mu\text{S/cm}$

APPENDIX 'E'

LICON TRANSVAP 150
LOG SHEET ON ROCKY FLATS POND WATER TESTS
JOB NO. 901

POND WATER *BW*

DATE: 9/24

| TIME: 11:30 | 10:00 | 10:30 | 11:00 | 11:30 | 12:00 | 12:30 | 1:00 | 1:30 | 2:00 |
|------------------------|---------|---------|---------|-------|-------|-------|-------|------|------|
| TEMPERATURES: | | | | | | | | | |
| T1 FEED SUPPLY | 82 | 82 | 82 | 82 | 82 | 83 | 83 | | |
| T2 FEED TO VC | 154 | 150 | 157 | 160 | 128 | 140 | 120 | | |
| T3 VC RECYCLE FEED | 188 | 186 | 179 | 180 | 168 | 176 | 164 | | |
| T4 BLOWDOWN TO MEMS | 84 | 84 | 84 | 84 | 166 | 162 | 168 | | |
| T5 VC SUCTION | 167 | 174 | 175 | 176 | 167 | 170 | 169 | | |
| T6 VC VENT | 184 | 173 | 191 | 193 | 182 | 187 | 184 | | |
| T7 VC CHEST | 187 | 191 | 193 | 195 | 188 | 190 | 186 | | |
| T8 VC EDUCTOR DISCH. | 193 | 172 | 178 | 180 | 180 | 192 | 176 | | |
| T9 VC DISTILLATE IN HX | 161 | 159 | 167 | 171 | 173 | 173 | 165 | | |
| T10 VC DIST. OUT HX | 97 | 102 | 109 | 106 | 96 | 100 | 94 | | |
| T11 1ST FLASH VAPOR | 182 | 180 | 180 | 178 | 182 | | 174 | | |
| T12 2ND FLASH VAPOR | 169 | 169 | 169 | 164 | 170 | 1 | 166 | | |
| T13 3RD FLASH VAPOR | 126 | 130 | 126 | 128 | 126 | 9 | 129 | | |
| T14 4TH FLASH VAPOR | 64 | 107 | 107 | 108 | 107 | | 122 | | |
| T15 COOLANT INLET | 58 | 86 | 86 | 70 | 83 | 4 | 82 | | |
| T16 COOLANT OUTLET | 60 | 100 | 97 | 74 | 93 | 8 | 88 | | |
| T17 4TH FLASH CONC. | 91 | 111 | 105 | 115 | 105 | 10 | 112 | | |
| T18 4TH FLASH FEED | 110 | 122 | 121 | 127 | 121 | 11 | 125 | | |
| T19 3RD FLASH CONC. | 136 | 142 | 134 | 131 | 134 | 11 | 141 | | |
| T20 3RD FLASH FEED | 156 | 158 | 158 | 152 | 155 | 11 | 154 | | |
| T21 2ND FLASH CONC. | 165 | 164 | 166 | 164 | 168 | 11 | 165 | | |
| T22 FEED TO HTR. | 176 | 172 | 175 | 171 | 176 | 11 | 170 | | |
| T23 OUTPUT FROM HTR. | 192 | 182 | 185 | 181 | 187 | | 176 | | |
| F1 FIRST STAGE RECYCLE | 406 gpm | 406 gpm | 406 gpm | 40 | 40 | | 40 | | |
| F2 VC FEED RATE | 3 1/2 | 3 1/2 | 3 | 3 | 3 | | 3 | | |
| F3 VC BLOWDOWN | - | - | - | - | 1.6 | | 1.6 | | |
| F4 VC RECYCLE | 3 | 3 1/2 | 3 | 3 | 3 | | 3 | | |
| H1 VC BRINE WEIR | 1 1/4" | 1 1/4" | 1" | 1" | 1" | | 1" | | |
| H2 3RD STAGE WEIR | 3" | 3" | 3" | 3" | 3" | | 3" | | |
| H3 4TH STAGE WEIR | 3" | 3" | 3" | 3" | 3" | | 3" | | |
| FEED TANK LEVEL | 1100 | 1075 | 1000 | 975 | 850 | 775 | 725 | 775 | |
| M1 VC DISTILLATE | 2072 | 2133 | 2187 | 2205 | 2291 | 2329 | 2260 | | |
| M2 MEMS DISTILLATE | 17238 | 17275 | 17310 | 17326 | 17371 | 17376 | 17400 | | |
| M3 COMBINED DIST. | 30 | 78 | 89 | 82 | 81 | 45 | 53 | | |
| V VOLTAGE | 475 | 475 | | 475 | 475 | | 475 | | |
| A AMPS | 52.6 | 56.3 | 38.2 | 40.2 | 58 | | 56.4 | | |

LOG SHEET FOR WATER SAMPLES

JOB ORDER 901

| | | | | | | | | | |
|----------------------|---------|-------|-------|-------|-------|-------|-------|-------|--|
| DATE: | 9/24/90 | | | | | | | | |
| TIME: | 930 | 1000 | 1030 | 1100 | 1130 | 1200 | 1230 | 100 | |
| POND A | | | | | | | | | |
| CONDUCTIVITY FEED | | | | | | | | | |
| DIST. | | | | | | | | | |
| CONC. | | | | | | | | | |
| pH | | | | | | | | | |
| FEED | | | | | | | | | |
| DIST. | | | | | | | | | |
| CONC. | | | | | | | | | |
| POND BN | | | | | | | | | |
| CONDUCTIVITY FEED #4 | 13.99 | 14.01 | 14.04 | 14.07 | 14.07 | 14.08 | 14.11 | 14.10 | |
| DIST. #5 | | 0.44 | 0.18 | 0.28 | 0.28 | 0.25 | 0.58 | 0.29 | |
| CONC. #6 | | 16.94 | 17.07 | 18.19 | 19.32 | 22.0+ | 22.0+ | 22.0+ | |
| pH | | | | | | | | | |
| FEED #4 | 9.7 | 9.7 | 9.7 | 9.7 | 9.7 | 9.7 | 9.7 | 9.7 | |
| DIST. #5 | | 6.0 | 5.5 | 6.0 | 5.5 | 6.0 | 6.5 | 6.3 | |
| CONC. #6 | | 8.1 | 7.9 | 7.8 | 7.7 | 7.8 | 7.6 | 7.7 | |
| POND BC | | | | | | | | | |
| CONDUCTIVITY FEED | | | | | | | | | |
| DIST. | | | | | | | | | |
| CONC. | | | | | | | | | |
| pH | | | | | | | | | |
| FEED | | | | | | | | | |
| DIST. | | | | | | | | | |
| CONC. | | | | | | | | | |
| POND BS | | | | | | | | | |
| CONDUCTIVITY FEED | | | | | | | | | |
| DIST. | | | | | | | | | |
| CONC. | | | | | | | | | |
| pH | | | | | | | | | |
| FEED | | | | | | | | | |
| DIST. | | | | | | | | | |
| CONC. | | | | | | | | | |

Acidifying @ 1230 after these readings

All Conductivity measured MS/cm

POND water BN

Rocky Flats, Col

9/24/90

Richard W. Boothe

| TIME | 930 | 1000 | 1030 | 1100 | 1130 | 1200 | 1230 | 100 | 130 | 200 | 230 |
|-------------------------------|-------|--------|--------|--------|--------|--------|--------|--------|-----|-----|-----|
| VC FEED PH | 9.7 | 9.7 | 9.7 | 9.7 | 9.7 | 9.7 | 9.7 | 9.7 | | | |
| FLASH DIST/COND. Tank | 0.12 | 0.67 | 0.42 | 0.28 | 0.20 | 0.14 | 0.12 | 0.10 | | | |
| FLASH DIST/PH " | 8.0 | 7.1 | 6.3 | 6.4 | 6.3 | 6.4 | 7.8 | 7.1 | | | |
| VC DIST /COND. Tank | 0.10 | 0.07 | 0.06 | 0.05 | 0.05 | 0.06 | 0.05 | 0.06 | | | |
| VC DIST/PH " | 5.7 | 5.5 | 5.2 | 5.3 | 5.1 | 5.4 | 5.3 | 5.4 | | | |
| DIST/COMBINED COND. | | 0.44 | 0.18 | 0.28 | 0.28 | 0.25 | 0.58 | 0.29 | | | |
| DIST/COMBINED PH | | 6.0 | 5.5 | 6.0 | 5.5 | 6.0 | 6.5 | 6.3 | | | |
| FLASH CONC. PH | | 8.1 | 7.9 | 7.9 | 7.7 | 7.8 | 7.6 | 7.7 | | | |
| VC CONC. PH Tank | | 8.0 | 8.4 | 8.6 | 8.6 | 8.8 | 6.5 | 8.6 | | | |
| (Tank) Feed (Cond.) | 13.99 | 14.01 | 14.04 | 14.07 | 14.07 | 14.08 | 14.11 | 14.10 | | | |
| Flash Concentrate (Cond.) | | 16.94 | 17.07 | 18.19 | 19.32 | 20000+ | 20000+ | 20000+ | | | |
| VC Dist Sample Pot (Cond.) | 0.02 | 0.02 | 0.02 | 0.03 | 0.04 | 0.05 | 0.11 | 0.04 | | | |
| VC Dist Sample Pot (PH) | 8.0 | 8.2 | 7.4 | 7.6 | 7.5 | 7.4 | 6.3 | 7.7 | | | |
| Flash DIST Sample Pot (Cond.) | | 0.13 | 0.07 | 0.06 | 0.05 | 0.04 | 0.04 | 0.03 | | | |
| Flash DIST Sample Pot (PH) | | 8.9 | 8.9 | 7.9 | 8.8 | 7.0 | 7.9 | 7.2 | | | |
| VC Conc. Tank (Cond.) | | 20000+ | 20000+ | 20000+ | 20000+ | 20000+ | 20000+ | 20000+ | | | |

All conductivity measured ms/cm

200 .5# EDTA added to VC concentrate Tank.
 PH @ 12:20. 6.5 @ 12:30 8.5

2:20 VC shut down L/W/heater
 2:21 VC Back on line

12:35 added .5# EDTA to VC conc. tank
 PH @ 12:35 6.5

2:35 VC shut down H/L
 2:38 VC Back on line

2:50 VC sample pot (cond.) 0.04 ms/cm (PH) 7.2

3:10 VC + Flash unit shut down By Danny, No further testing today!

5:00 VC Conc high side - 43 mS some precipitate (MgOH?)
 4th Stage Flash - 26 mS " " (MgOH?)

93

LICON TRANSVAP 150
LOG SHEET ON ROCKY FLATS POND WATER TESTS
JOB NO. 901

POND WATER RW TANK #1

DATE: 9/25/64

| TIME: 2:00 | 2:30 | 3:00 | 3:30 | 4:00 | 4:30 | 5:00 | 5:30 | 6:00 | 6:30 | 7:00 |
|------------------------|--------|--------|-------|-------|-------|-------|-------|-------|-------|------|
| TEMPERATURES: | | | | | | | | | | |
| T1 FEED SUPPLY | 84 | 89 | 84 | 84 | | 84 | 84 | 85 | 85 | |
| T2 FEED TO VC | 120 | 128 | 162 | 130 | | 108 | 154 | 152 | 152 | |
| T3 VC RECYCLE FEED | 182 | 176 | 174 | 179 | | 159 | 177 | 172 | 178 | |
| T4 BLOWDOWN TO MEMS | 134 | 134 | 127 | 135 | | 164 | 160 | 158 | 163 | |
| T5 VC SUCTION | 170 | 170 | 171 | 174 | | 165 | 174 | 168 | 176 | |
| T6 VC VENT | 190 | 190 | 198 | 194 | | 184 | 194 | 187 | 196 | |
| T7 VC CHEST | 192 | 192 | 200 | 196 | | 186 | 196 | 189 | 198 | |
| T8 VC EDUCTOR DISCH. | 180 | 180 | 187 | 177 | | 180 | 188 | 183 | 189 | |
| T9 VC DISTILLATE IN HX | 170 | 169 | 162 | 163 | | 172 | 177 | 176 | 186 | |
| T10 VC DIST. OUT HX | 93 | 101 | 118 | 95 | | 94 | 138 | 124 | 110 | |
| T11 1ST FLASH VAPOR | 170 | 170 | 183 | 180 | | 169 | 162 | 165 | 166 | |
| T12 2ND FLASH VAPOR | 162 | | 175 | 171 | | 161 | 153 | 157 | 158 | |
| T13 3RD FLASH VAPOR | 135 | | 140 | 148 | | 134 | 131 | 129 | 131 | |
| T14 4TH FLASH VAPOR | 72 | | 134 | 124 | | 129 | 127 | 125 | 125 | |
| T15 COOLANT INLET | 62 | | 66 | | | 80 | 76 | 76 | 78 | |
| T16 COOLANT OUTLET | 66 | | 78 | | | 88 | 81 | 82 | 85 | |
| T17 4TH FLASH CONC. | 90 | | 134 | 144 | | 125 | 125 | 122 | 123 | |
| T18 4TH FLASH FEED | 100 | | 138 | 147 | | 131 | 129 | 127 | 128 | |
| T19 3RD FLASH CONC. | 142 | | 155 | 156 | | 145 | 132 | 132 | 140 | |
| T20 3RD FLASH FEED | 151 | | 172 | 160 | | 154 | 144 | 145 | 146 | |
| T21 2ND FLASH CONC. | 160 | | 174 | 166 | | 160 | 155 | 156 | 157 | |
| T22 FEED TO HTR. | 164 | | 180 | 171 | | 166 | 160 | 162 | 163 | |
| T23 OUTPUT FROM HTR. | 163 | | 187 | 125 | | 171 | 165 | 168 | 169 | |
| F1 FIRST STAGE RECYCLE | 40 gpm | 40 gpm | 40 | 40 | | 40 | 40 | 40 | 40 | |
| F2 VC FEED RATE | 2.5 | 2.5 | 3 | 3 | | 3 | 3 | 3 | 3 | |
| F3 VC BLOWDOWN | 1.6 | 1.6 | 1.6 | 1.6 | | 1.6 | 1.6 | 1.6 | 1.6 | |
| F4 VC RECYCLE | 3 | 3 | 3 | 3 | | 3 | 3 | 3 | 3 | |
| H1 VC BRINE WEIR | 1" | 1" | 1" | 1" | | 1" | 1" | 1" | 1" | |
| H2 3RD STAGE WEIR | 3" | 3" | 3" | 3" | | 3" | 3" | 3" | 3" | |
| H3 4TH STAGE WEIR | 3" | 3" | 3" | 3" | | 3" | 3" | 3" | 3" | |
| FEED TANK LEVEL | 550 | 500 | 450 | 400 | 350 | 300 | 250 | 200 | 150 | |
| M1 VC DISTILLATE | 8393 | 82440 | 82444 | 82530 | 82577 | 82610 | 82652 | 82686 | 82720 | |
| M2 MEMS DISTILLATE | 17419 | 17427 | 17434 | 17447 | 17460 | 17479 | 17490 | 17490 | 17519 | |
| M3 COMBINED DIST. | — | 55 | 64 | 49 | 60 | 52 | 53 | 34 | 63 | |
| V VOLTAGE | 475 | 475 | 475 | 475 | | 475 | 475 | 475 | 475 | |
| A AMPS | 53.3 | 46.3 | 44.1 | 52.7 | | 55.4 | 50.2 | 40 | 41.0 | |

Rocky Flats, Col

9/24/90

Richard W. Boothe

| TIME | 930 | 1000 | 1030 | 1100 | 1130 | 1200 | 1230 | 100 | 130 | 200 | 230 |
|-------------------------------|-------|--------|--------|--------|--------|--------|--------|--------|-----|-----|-----|
| VC FEED PH | 9.7 | 9.7 | 9.7 | 9.7 | 9.7 | 9.7 | 9.7 | 9.7 | | | |
| FLASH DIST/COND. Tank | 0.12 | 0.67 | 0.42 | 0.28 | 0.20 | 0.14 | 0.12 | 0.10 | | | |
| FLASH DIST/PH " | 8.0 | 7.1 | 6.3 | 6.4 | 6.3 | 6.4 | 7.8 | 7.1 | | | |
| VC DIST /COND. Tank | 0.10 | 0.07 | 0.06 | 0.05 | 0.05 | 0.06 | 0.05 | 0.06 | | | |
| VC DIST/PH " | 5.7 | 5.5 | 5.2 | 5.3 | 5.1 | 5.4 | 5.3 | 5.4 | | | |
| DIST/COMBINED COND. | | 0.44 | 0.18 | 0.28 | 0.28 | 0.25 | 0.58 | 0.29 | | | |
| DIST/COMBINED PH | | 6.0 | 5.5 | 6.0 | 5.5 | 6.0 | 6.5 | 6.3 | | | |
| FLASH CONC. PH | | 8.1 | 7.9 | 7.9 | 7.7 | 7.8 | 7.6 | 7.7 | | | |
| VC CONC. PH Tank | | 8.0 | 8.4 | 8.6 | 8.6 | 8.8 | 6.5 | 8.6 | | | |
| (Tank) Feed (Cond.) | 13.99 | 14.01 | 14.04 | 14.07 | 14.07 | 14.08 | 14.11 | 14.10 | | | |
| Flash Concentrate (Cond.) | | 16.94 | 17.07 | 18.19 | 19.32 | 20.04 | 20.00+ | 20.00+ | | | |
| VC Dist Sample Pot (Cond.) | 0.02 | 0.02 | 0.02 | 0.03 | 0.04 | 0.05 | 0.11 | 0.04 | | | |
| VC Dist Sample Pot (PH) | 8.0 | 8.2 | 7.4 | 7.6 | 7.5 | 7.4 | 6.3 | 7.7 | | | |
| Flash DIST Sample Pot (Cond.) | | 0.13 | 0.07 | 0.06 | 0.05 | 0.04 | 0.04 | 0.03 | | | |
| Flash DIST Sample Pot (PH) | | 8.9 | 8.9 | 7.9 | 8.8 | 7.0 | 7.9 | 7.2 | | | |
| VC Conc. Tank (Cond.) | | 20000+ | 20000+ | 20000+ | 20000+ | 20000+ | 20000+ | 20000+ | | | |

All conductivity measured ms/cm

200 .5# EDTA added to VC concentrate Tank.

PH @ 12:20. 6.5 @ 12:30 8.5

2:20 VC shut down L/W/heater

2:21 VC Back on line

12:55 added .5# EDTA to VC conc. tank
PH @ 12:35 6.5

2:35 VC shut down H/L

2:38 VC Back online

2:50 VC sample pot (cond.) 0.04 ms/cm (PH) 7.2

3:10 VC + Flash unit shut down by Danny, No further testing today!

5:00 VC Conc high side - 43 mS some precipitate (MgOH?)
4th Stage Flash - 26 mS " " (MgOH?)

93

Rocky Flats, Col.

9/25/90

2nd 3N Tank-1 (Heidi)

Richard W. Boothe

| TIME | 230 | 300 | 330 | 400 | 430 | 500 | 530 | 600 | 630 | 700 | 730 |
|-------------------------------|----------------------|-----------|-----------|-------------------|-----------|-----------------|-----------------|-----------------|-----------|-----|-----|
| VC FEED PH | 8.7 | 8.8 | 7.9 | 7.3 | 7.9 | 6.9 | 7.5 | 8.2 | 8.4 | | |
| FLASH DIST/COND. | 2.13 | 1.89 | 2.90 | 2.84 | 1.99# | 1.30 | 2.83 | 2.64 | 2.45 | | |
| FLASH DIST/PH | 6.7 | 7.1 | 6.7 | 6.8 | 6.4 | 6.7 | 6.7 | 6.4 | 6.4 | | |
| VC DIST /COND. | 0.05 | 0.05 | 0.04 | 0.04 | 0.05 | 0.04 | 0.04 | 0.05 | 0.05 | | |
| VC DIST/PH | 5.2 | 5.1 | 5.2 | 5.2 | 5.3 | 5.3 | 5.4 | 5.6 | 5.5 | | |
| DIST/COMBINED COND. | 0.06 | 0.93 | 2.04 | 0.07 | 0.97# | 1.14 | 0.09 | 0.39 | 0.20 | | |
| DIST/COMBINED PH | 5.6 | 6.0 | 5.1 | 5.3 | 5.9 | 6.2 | 5.5 | 5.8 | 5.7 | | |
| FLASH CONC. PH | 6.8 | 7.2 | 7.5 | 7.8 | 7.8 | 7.8 | 7.8 | 8.0 | 8.0 | | |
| VC CONC. PH | 8.4 | 8.5 | 8.5 | 8.5 | 8.7 | 8.6 | 8.7 | 8.8 | 8.8 | | |
| 4 Tank Feed (Cond.) | 14.27 | 14.29 | 14.29 | 14.19 | 14.18 | 14.09 | 14.01 | 14.03 | 14.01 | | |
| 6 Flash Concentrate (Cond.) | off scale 29,000+ | off scale | off scale | off scale 30.0 | off scale | off scale 42 | off scale 48 | off scale 47 | off scale | | |
| VC DIST Sample Pot (Cond.) | 0.02 | 0.03 | 0.03 | 0.03 | 0.03 | 0.02 | 0.02 | 0.03 | 0.03 | | |
| VC DIST Sample Pot (PH) | 7.6 | 7.1 | 7.6 | 7.9 | 7.5 | 7.4 | 7.5 | 7.6 | 7.7 | | |
| Flash DIST Sample Pot (Cond.) | 0.30 | 0.18 | 1.10* | 0.21 | 0.11# | 0.04 | 0.02 | 0.03 | 0.02 | | |
| Flash DIST Sample Pot (PH) | 6.7 | 6.8 | 8.8 | 6.7 | 6.6 | 6.8 | 6.5 | 7.0 | 7.1 | | |
| VC Concentrate Tank (Cond.) | off scale 40-41 | off scale | off scale | off scale | off scale | off scale 51 | off scale | off scale 38 | off scale | | |

All Conductivity measured ms/cm

* Last Boiler - Carry-over.

() VC Conc High Side @ 1700 = 51 ms

Flash badly contaminated because of boiler failures
and CO₂ build-up due to acid reaction see pot readings
Hooked up separate auxiliary exhaust to 2nd Stage Flash

| | | | |
|----------------------|-------------|-------------|-------------|
| 3rd Stage Flash Conc | 62ms @ 1730 | 78ms @ 1800 | 85ms @ 1830 |
| 4th " " " | 48ms " " | 45ms @ 1800 | 47 " " " |

| TIME: 9:30 | 10:00 | 10:30 | 11:00 | 11:30 | 12:00 | 12:30 | 1:00 | 1:30 | 2:00 |
|--------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| TEMPERATURES: | | | | | | | | | |
| T1 FEED SUPPLY | 77 | 77 | 77 | 77 | 77 | 77 | 77 | 77 | 77 |
| T2 FEED TO VC | 142 | 175 | 137 | 154 | 146 | 142 | 131 | 131 | 166 |
| T3 VC RECYCLE FEED | 173 | 179 | 169 | 178 | 173 | 167 | 167 | 167 | 176 |
| T4 BLOWDOWN TO MEMS | 150 | 165 | 165 | 167 | 168 | 166 | 166 | 166 | 164 |
| T5 VC SUCTION | 170 | 176 | 170 | 175 | 175 | 170 | 169 | 169 | 175 |
| T6 VC VENT | 189 | 198 | 191 | 197 | 196 | 190 | 189 | 189 | 197 |
| T7 VC CHEST | 191 | 201 | 192 | 199 | 197 | 191 | 190 | 190 | 199 |
| T8 VC EDUCTOR DISCH. | 183 | 186 | 182 | 189 | 184 | 178 | 180 | 180 | 187 |
| T9 VC DISTILLATE IN HX | 176 | 180 | 172 | 180 | 175 | 176 | 172 | 172 | 174 |
| T10 VC DIST. OUT HX | 89 | 94 | 90 | 92 | 92 | 92 | 90 | 90 | 110 |
| T11 1ST FLASH VAPOR | 168 | 177 | 180 | 178 | 177 | 176 | 176 | 176 | 176 |
| T12 2ND FLASH VAPOR | 160 | 161 | 167 | 165 | 165 | 164 | 164 | 164 | 165 |
| T13 3RD FLASH VAPOR | 115 | 123 | 132 | 132 | 127 | 128 | 128 | 128 | 129 |
| T14 4TH FLASH VAPOR | 106 | 114 | 123 | 118 | 115 | 120 | 120 | 118 | 118 |
| T15 COOLANT INLET | 83 | 80 | 83 | 88 | 87 | 85 | 85 | 84 | 84 |
| T16 COOLANT OUTLET | 92 | 99 | 93 | 103 | 100 | 95 | 95 | 96 | 96 |
| T17 4TH FLASH CONC. | 95 | 109 | 120 | 117 | 115 | 116 | 116 | 116 | 116 |
| T18 4TH FLASH FEED | 109 | 120 | 129 | 127 | 123 | 125 | 125 | 125 | 125 |
| T19 3RD FLASH CONC. | 120 | 126 | 139 | 140 | 136 | 134 | 134 | 134 | 134 |
| T20 3RD FLASH FEED | 139 | 142 | 151 | 151 | 150 | 150 | 150 | 150 | 150 |
| T21 2ND FLASH CONC. | 160 | 161 | 166 | 165 | 165 | 162 | 162 | 162 | 162 |
| T22 FEED TO HTR. | 162 | 164 | 166 | 165 | 165 | 165 | 165 | 165 | 165 |
| T23 OUTPUT FROM HTR. | 174 | 171 | 173 | 172 | 172 | 171 | 171 | 171 | 171 |
| F1 FIRST STAGE RECYCLE | 40 | 40 | 40 | 40 | 40 | 40 | 40 | 40 | 40 |
| F2 VC FEED RATE | 3 1/2 | 3 1/2 | 3 1/2 | 3 1/2 | 3 1/2 | 3 1/2 | 3 1/2 | 3 1/2 | 3 1/2 |
| F3 VC BLOWDOWN | 1.6 | 1.6 | 1.6 | 1.6 | 1.6 | 1.6 | 1.6 | 1.6 | 1.6 |
| F4 VC RECYCLE | 2 1/4 | 3 1/2 | 3 1/2 | 3 1/2 | 3 1/2 | 3 1/2 | 3 1/2 | 3 1/2 | 3 1/2 |
| H1 VC BRINE WEIR | 1" | 1" | 1" | 1" | 1" | 1" | 1" | 1" | 1" |
| H2 3RD STAGE WEIR | 3" | 3" | 3" | 3" | 3" | 3" | 3" | 3" | 3" |
| H3 4TH STAGE WEIR | 3" | 3" | 3" | 3" | 3" | 3" | 3" | 3" | 3" |
| FEED TANK LEVEL | 1250 | 1200 | 1150 | 1050 | 980 | 900 | 835 | 770 | 718 |
| M1 VC DISTILLATE 20965 | 20993 | 21036 | 21079 | 21126 | 21170 | 21215 | 21258 | 21304 | 21339 |
| M2 MEMS DISTILLATE 17552 | - | 17560 | 17585 | 17615 | 17641 | 17674 | 17704 | 17733 | 17750 |
| M3 COMBINED DIST. | | 51 | 68 | 77 | 70 | 78 | 65 | 85 | 52 |
| V VOLTAGE | 475 | 475 | 475 | 475 | 475 | 475 | 475 | 475 | 475 |
| A AMPS | 58.5 | 41 | 40.9 | 39 | 57.3 | 38.2 | 58.9 | 59.1 | 41.2 |
| KW KILOWATTS | | | | | | | | | |
| PF POWER FACTOR | 0.81 | 0.7 | 0.7 | 0.7 | 0.7 | 0.7 | 0.7 | 0.7 | 0.7 |

MEMS DISTILLATE
 VC DISTILLATE
 VC RECYCLE
 VC FEED
 VC BLOWDOWN
 VC RECYCLE
 VC BRINE WEIR
 VC 3RD STAGE WEIR
 VC 4TH STAGE WEIR
 VC FEED TANK LEVEL
 VC DISTILLATE
 MEMS DISTILLATE
 COMBINED DIST.
 VOLTAGE
 AMPS
 KW
 PF

| TIME: | 2:30 | 3:00 | 3:30 | 4:00 | 4:30 | 5:00 | 5:30 | 6:00 | 6:30 |
|------------------------|-------|-------|------|------|-------|-------|--------|-------|--------|
| TEMPERATURES: | | | | | | | | | |
| T1 FEED SUPPLY | 87 | | | | 80 | 82 | 82 | 82 | 82 |
| T2 FEED TO VC | 134 | | | | 144 | 142 | 142 | 150 | 152 |
| T3 VC RECYCLE FEED | 166 | | | | 170 | 167 | 168 | 167 | 167 |
| T4 BLOWDOWN TO MEMS | 164 | | | | 166 | 166 | 170 | 167 | 166 |
| T5 VC SUCTION | 170 | | | | 170 | 170 | 173 | 170 | 170 |
| T6 VC VENT | 189 | | | | 192 | 192 | 194 | 192 | 192 |
| T7 VC CHEST | 190 | | | | 194 | 194 | 198 | 194 | 194 |
| T8 VC EDUCTOR DISCH. | 179 | | | | 186 | 181 | 182 | 184 | 184 |
| T9 VC DISTILLATE IN HX | 174 | | | | 176 | 170 | 170 | 172 | 169 |
| T10 VC DIST. OUT HX | 90 | | | | 112 | 92 | 92 | 92 | 92 |
| T11 1ST FLASH VAPOR | 176 | | | | 178 | 171 | 171 | 172 | 172 |
| T12 2ND FLASH VAPOR | 165 | | | | 168 | 165 | 165 | 166 | 167 |
| T13 3RD FLASH VAPOR | 127 | | | | 127 | 128 | 128 | 130 | 130 |
| T14 4TH FLASH VAPOR | 122 | | | | 113 | 117 | 117 | 117 | 118 |
| T15 COOLANT INLET | 85 | | | | 86 | 86 | 86 | 86 | 86 |
| T16 COOLANT OUTLET | 92 | | | | 98 | 98 | 98 | 101 | 100 |
| T17 4TH FLASH CONC. | 115 | | | | 111 | 114 | 114 | 116 | 116 |
| T18 4TH FLASH FEED | 124 | | | | 122 | 124 | 124 | 127 | 127 |
| T19 3RD FLASH CONC. | 135 | | | | 133 | 136 | 136 | 138 | 138 |
| T20 3RD FLASH FEED | 150 | | | | 150 | 148 | 148 | 150 | 152 |
| T21 2ND FLASH CONC. | 165 | | | | 165 | 164 | 164 | 165 | 166 |
| T22 FEED TO HTR. | 165 | | | | 165 | 164 | 164 | 165 | 166 |
| T23 OUTPUT FROM HTR. | 171 | | | | 173 | 172 | 172 | 174 | 174 |
| F1 FIRST STAGE RECYCLE | 40 | | | | 40 | 40 | 40 | 40 | 40 |
| F2 VC FEED RATE | 3 1/2 | | | | 3 1/2 | 3 1/2 | 3 1/2 | 3 1/2 | 3 1/2 |
| F3 VC BLOWDOWN | 1.6 | | | | 1.6 | 1.6 | 1.6 | 1.6 | 1.6 |
| F4 VC RECYCLE | 3 | | | | 3 | 3 | 3 1/2 | 3 1/2 | 3 1/2 |
| H1 VC BRINE WEIR | 1" | | | | 1" | 1" | 1 1/4" | 1" | 1 1/4" |
| H2 3RD STAGE WEIR | 3" | | | | 3" | 3" | 3 1/4" | 3" | 3" |
| H3 4TH STAGE WEIR | 3" | | | | 3" | 3" | 3 1/4" | 3" | 3 1/4" |
| FEED TANK LEVEL | 643 | | | | 558 | 484 | 421 | 343 | 283 |
| M1 VC DISTILLATE | 21379 | 21419 | | | 21458 | 21506 | 21543 | 21585 | 21622 |
| M2 MEMS DISTILLATE | 17785 | 17814 | | | 17860 | 17886 | 17910 | 17948 | 17971 |
| M3 COMBINED DIST. | 75 | | | | 85 | 74 | 63 | 48 | 60 |
| V VOLTAGE | 475 | | | | 475 | 475 | 475 | 475 | 475 |
| A AMPS | 61.1 | | | | 40.1 | 59.9 | 59 | 39.8 | 28.5 |
| KW KILOWATTS | | | | | | | | | |
| PF POWER FACTOR | .872 | | | | .7 | | | | |

CONDENSER
 TO
 FEED
 TANK
 4:00
 4:10
 4:20
 4:30
 4:40
 4:50
 5:00
 5:10
 5:20
 5:30
 5:40
 5:50
 6:00
 6:10
 6:20
 6:30
 6:40
 6:50
 7:00

Rocky Flats, Col.

POND BN Batch #2

9/26/90

Richard W. Boothe

| TIME | 9:30 | 10:00 | 10:30 | 11:00 | 11:30 | 12:00 | 12:30 | 1:00 | 1:30 | 2:00 | 2:30 |
|------------------------------------|-------|-----------|-----------|-------|-----------|-----------|-----------|-----------|-----------|-----------|-------|
| VC FEED PH | | 8.6 | 8.3 | 8.4 | 8.5 | 8.6 | 8.7 | 8.7 | 8.7 | 8.7 | 8.8 |
| FLASH DIST/COND. | | 0.28 | 0.16 | 0.11 | 0.09 | 0.04 | 0.03 | 0.03 | 0.02 | 0.01 | 0.01 |
| FLASH DIST/PH | | 6.2 | 5.7 | 5.4 | 5.4 | 5.3 | 5.3 | 5.2 | 5.2 | 5.2 | 5.0 |
| VC DIST /COND. | | 0.05 | 0.07 | 0.07 | 0.06 | 0.07 | 0.06 | 0.07 | 0.06 | 0.07 | 0.06 |
| VC DIST/PH | | 5.3 | 5.4 | 5.5 | 5.4 | 5.5 | 5.4 | 5.5 | 5.5 | 5.4 | 5.4 |
| DIST/COMBINED COND. | | 0.26 | 0.21 | 0.24 | 0.18 | 0.17 | 0.14 | 0.13 | 0.15* | 0.04 | 0.04 |
| DIST/COMBINED PH | | 5.9 | 5.8 | 5.7 | 5.5 | 5.5 | 5.7 | 5.6 | 5.6 | 5.4 | 5.5 |
| FLASH CONC. PH | | 8.5 | 8.3 | 8.3 | 8.4 | 8.4 | 8.4 | 8.4 | 8.4 | 8.4 | 8.4 |
| VC CONC. PH | | 8.7 | 8.7 | 8.8 | 8.7 | 8.8 | 8.8 | 8.8 | 8.8 | 8.8 | 8.8 |
| 4-TANK FEED (COND) | | 13.59 | 13.55 | 13.57 | 13.59 | 13.58 | 13.59 | 13.61 | 13.62 | 13.61 | 13.63 |
| 6-FLASH CONCENTRATE (COND) | | off scale | off scale | 62.5 | off scale | off scale | 88.7 | off scale | off scale | off scale | 125.7 |
| VC DISTILLATE SAMPLE PH (COND) | | 0.03 | 0.04 | 0.05 | 0.03 | 0.04 | 0.06 | 0.03 | 0.03 | 0.03 | 0.03 |
| VC DISTILLATE SAMPLE POT (PH) | | 7.6 | 7.6 | 7.4 | 7.9 | 7.7 | 7.7 | 7.7 | 7.9 | 7.8 | 7.8 |
| FLASH DISTILLATE SAMPLE TOT (COND) | | 0.06 | 0.04 | 0.02 | 0.01 | 0.01 | 0.01 | 0.008 | 0.01 | 0.009 | 0.01 |
| FLASH DISTILLATE SAMPLE POT (PH) | | 9.1 | 7.8 | 6.5 | 6.2 | 6.3 | 6.8 | 6.3 | 5.7 | 5.6 | 6.2 |
| VC CONCENTRATE TANK (COND) | 27.5 | off scale | off scale | 36.75 | off scale | off scale | off scale | off scale | 25.0 | off scale | 35.0 |
| ED TANK (PH) | 7.7 | 8.3 | 8.3 | 8.5 | 8.5 | 8.6 | 8.7 | 8.8 | 8.8 | 8.8 | 8.8 |
| FEED TANK (COND) | 13.58 | 13.58 | 13.54 | 13.55 | 13.57 | 13.55 | 13.57 | 13.56 | 13.59 | 13.61 | 13.62 |

- ALL Conductivity measured mS/cm -

8:50 9# EDTA Added to feed tank

Before EDTA PH 9.7 COND. 13.12

After EDTA PH 8.1 COND. 13.58

* Note - Prior to 2:00 reading, found leaky valve to Dist Line from Conc. Tank

2:55 VC shut down

4:00 VC Back on line

Rocky Flats, Col Pond BN
Batch #2

9/26/90

Richard W. Boothe

| TIME | 4:30 | 5:00 | 5:30 | 6:00 | 6:30 | 7:00 | 7:30 | 8:00 | 8:30 | 9:00 |
|------------------------------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|------|
| VC FEED PH | 8.9 | 8.8 | 8.9 | 8.9 | 9.0 | 9.0 | 9.0 | 9.0 | 9.0 | |
| FLASH DIST/COND. | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | |
| FLASH DIST/PH | 5.0 | 5.0 | 5.2 | 5.0 | 5.1 | 5.2 | 5.2 | 5.1 | 5.2 | |
| VC DIST /COND. | 0.07 | 0.06 | 0.06 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 | |
| VC DIST/PH | 5.5 | 5.4 | 5.3 | 5.5 | 5.6 | 5.5 | 5.5 | 5.4 | 5.4 | |
| DIST/COMBINED COND. | 0.06 | 0.07 | 0.06 | 0.06 | 0.06 | 0.07 | 0.07 | 0.07 | 0.07 | |
| DIST/COMBINED PH | 5.7 | 5.6 | 5.6 | 5.4 | 5.5 | 5.4 | 5.3 | 5.4 | 5.4 | |
| FLASH CONC. PH | 8.4 | 8.2 | 8.3 | 8.3 | 8.3 | 8.3 | 8.3 | 8.3 | 8.3 | |
| VC CONC. PH | 8.8 | 8.8 | 8.6 | 8.7 | 8.7 | 8.8 | 8.8 | 8.9 | 8.9 | |
| TANK FEED (COND) | 13.63 | 13.66 | 13.67 | 13.69 | 13.71 | 13.68 | 13.67 | 13.68 | 13.80 | |
| FLASH CONCENTRATE (COND) | * 153 | off scale | off scale | off scale | 168 | off scale | off scale | off scale | off scale | |
| VC DISTILLATE SAMPLE TOT (COND) | 0.05 | 0.04 | 0.03 | 0.03 | 0.04 | 0.04 | 0.05 | 0.03 | 0.03 | |
| VC DISTILLATE SAMPLE TOT (PH) | 7.8 | 7.6 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 7.6 | |
| FLASH DISTILLATE SAMPLE TOT (COND) | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | |
| FLASH DISTILLATE SAMPLE TOT (PH) | 7.3 | 6.6 | 6.6 | 6.8 | 6.8 | 6.5 | 6.5 | 6.7 | 6.1 | |
| VC CONCENTRATE TANK (COND) | off scale | |
| FEED TANK (PH) | 8.9 | 8.8 | 8.9 | 8.9 | 8.9 | 9.0 | 9.0 | 9.0 | 9.0 | |
| FEED TANK (COND) | 13.61 | 13.63 | 13.63 | 13.64 | 13.64 | 13.64 | 13.66 | 13.66 | 13.72 | |

- All conductivity measured mS/cm

* @ 1630 3rd Stage Tank 156.20 mS at end of test 118.4 mS

* @ 1815 4th Stage Tank 167.520 mS " 222.8 mS

8:45 pm VC shut down pumping to Flash.



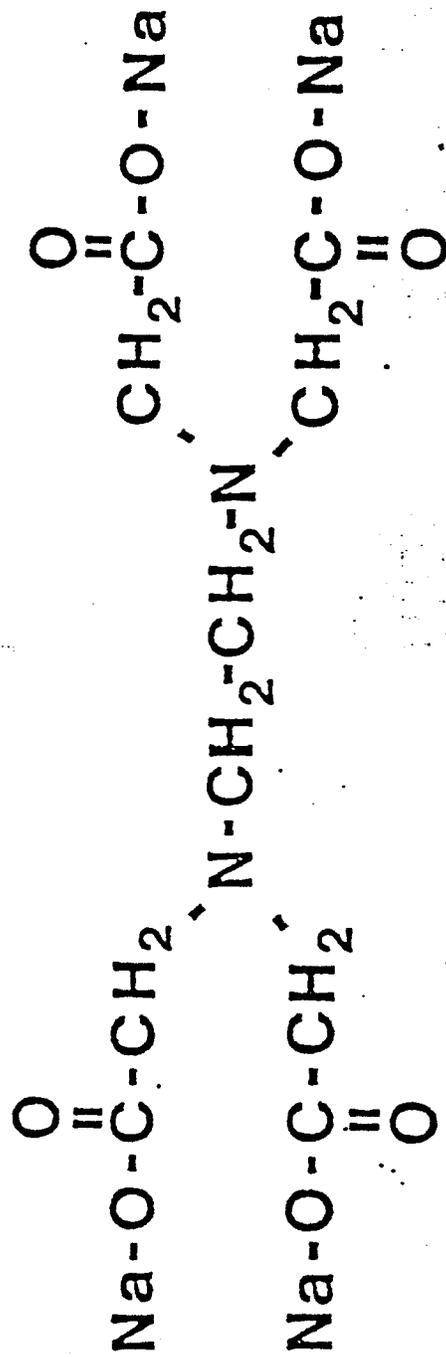


Figure 3a. Tetrasodium salt of ethylenediaminetetraacetic acid.

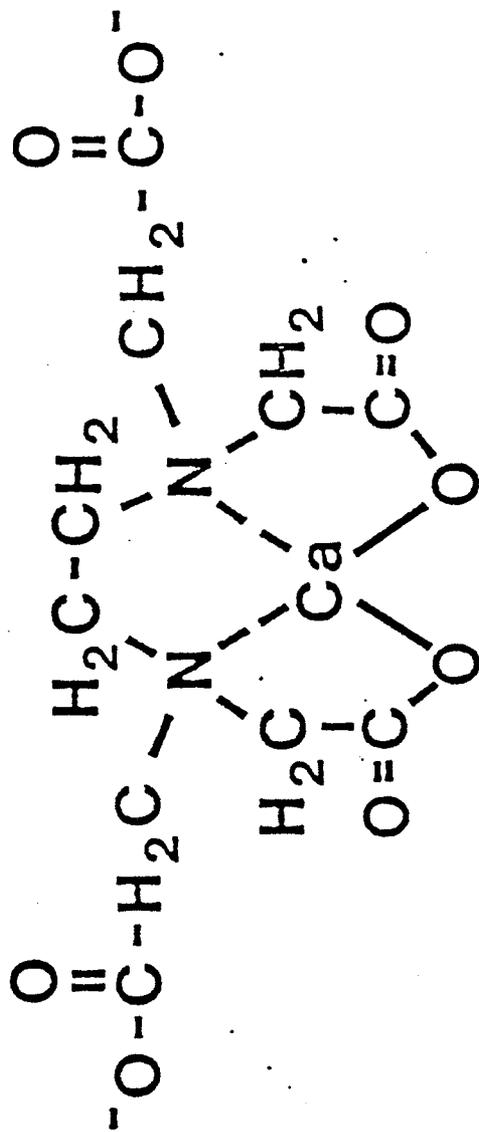


Figure 3b. Calcium chelate of ethylenediaminetetraacetate.

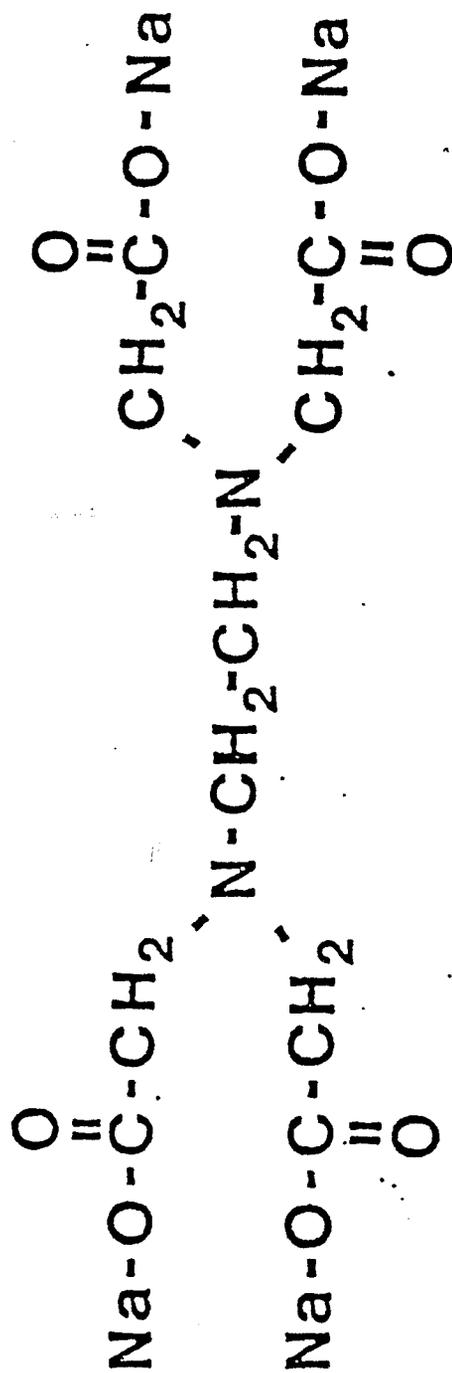


Figure 3a. Tetrasodium salt of ethylenediaminetetraacetic acid.